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## **INTRODUCTION**

The demand for standard semiconductor devices increased considerably in the last 5 - 6 years with introductions of VHF mobile radio and cordless telephones.

New developments in UHF (450 - 900 MHz) cellular radio and cordless telephones has generated a need for highly specialised devices and R.F. modules.

The fast-growing European market, notably based on TACS, NMT, CNET and CEPT standards calls for a dedicated device selector guide.

This brochure presents (under a single cover) a compilation of summarised information found on the front pages of data sheets related to Motorola Radio Communication products and devices.

Detailed technical data is available in data books, data sheets and specific application notes. Copies of data sheets and application notes can be obtained from Motorola Sales Office or distributors listed on the back cover.



**Alpha/Numeric List of Products**



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**List of Products by Function**



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# **Selector Guides for RF Modules and Discretes**

**RF Selector Guide**

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# SELECTOR GUIDES FOR RF MODULES AND DISCRETES

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- \* GENERAL PURPOSE WIDEBAND HYBRID AMPLIFIERS
- \* 407 – 512 MHZ UHF FM POWER TRANSISTORS
- \* 806 – 960 MHZ FM POWER TRANSISTORS
- \* 136 – 225 MHZ FM POWER TRANSISTORS
  
- \* 407 – 512 MHZ UHF RM POWER TRANSISTORS
- \* 806 – 960 MHZ UHF FM POWER TRANSISTORS
- \* 136 – 225 MHZ UHF FM POWER TRANSISTORS
  
- \* RF LOW NOISE AMPLIFIER TRANSISTORS
- \* FIELD EFFECT TRANSISTORS
  
- \* TUNING DIODES
- \* HYPER ABRUPT DIODES UHF/VHF
- \* SCHOTTKY DIODES
- \* PIN DIODES

LAND MOBILE POWER HYBRID AMPLIFIERS						
Device Type	P Out Watts	P In Watts	Freq. MHZ	Power Gain dB Min	V CC Volts	Package
A MHW709	7.5	0.1	400-512	18.8	12.5	700-03
A MHW710	13	0.15	400-512	19.4	12.5	700-03
B MHW720	20	0.15	400-470	21	12.5	700-03
B MHW720A+	20	0.15	400-470	21	12.5	700-03
C MHW802	2.2	0.05	825-915	20.4	9.5	784-01
D MHW808	7.5	0.25	806-950	14.8	12.5	297A-05
D MHW808A	7.5	0.03	806-950	24	12.5	301C-01
E MHW812	12	0.5	890-915	13.8	12.5	297A-06
D MHW820	20	0.25	806-950	19	12.5	301B-02

A: Available for 400-440 MHZ (-1); 440-470 MHZ (-2); 470-512 MHZ (-3)

B: Available for 400-440 MHZ (-1); 440-470 MHZ (-2)

C: Available for 825-845 MHZ (-1); 890-915 MHZ (-2)

D: Available for 806-870 MHZ (-1); 806-890 MHZ (-2); 870-950 MHZ (-3)

E: Available for 890-915 MHZ (-3)

+ Designed for Wide Range P Out Level Control

4

GENERAL PURPOSE WIDEBAND HYBRID AMPLIFIERS — 50 OHMS TO-39 PACKAGE					
Device Type	Frequency Range	Gain dB Min/Typ	VCC Volts	Output Level 1 dB Compression DBM Typ	Noise Fig @250 MW D
MWA110	0.1-400	13/14	2.9	-2.5	4
MWA120	0.1-400	13/14	5	8.2	5.5
MWA130	0.1-400	13/14	5.5	18	7
MWA210	0.1-500	9/10	1.75	1.5	6
MWA220	0.1-600	9/10	3.2	10.5	6.5
MWA230	0.1-600	9/10	4.4	18.5	7.5
MWA310	0.1-1000	7/8	1.6	3.5	6.5
MWA320	0.1-1000	7/8	2.9	11.5	6.7
MWA330	0.1-1000	-/6.2	4	15.2	9

**407-512 MHZ UHF FM POWER TRANSISTORS**

Device Type	P Out Watts	P In Watts	Power Gain dB Min	V CC Volts	Package
MRF629	2	0.32	8	12.5	TO-39
MRF630	3	0.33	9.5	12.5	TO-39
2N5944	2	0.25	9	12.5	244-04
2N5945	4	0.64	8	12.5	244-04
2N5946	10	2.5	6	12.5	244-04
MRF641	15	3.75	7.8	12.5	316-01
MRF644	25	5.9	6.2	12.5	316-01
MRF646	40	13.3	4.8	12.5	316-01
MRF648	60	22	4.4	12.5	316-01

**806-960 MHZ FM POWER TRANSISTORS**

Device Type	P Out Watts	P In Watts	Power Gain dB Min	V CC Volts	Package
MRF837	1.75	0.125	8	12.5	MACRO-X
MRF557	1.5	0.25	8	12.5	317D-01
MRF839	3	0.5	8	12.5	305-01
MRF841	5	0.7	8.5	12.5	244-04
MRF840	10	2.5	6	12.6	319-04
MRF843	15	3	7	12.5	244-04
MRF842	20	5	6	12.5	319-04
MRF844	30	9	5.2	12.5	319-04
MRF846	40	15	4.3	12.5	319-04
MRF848	60	25	4	12.5	333A
MRF890	2	0.25	9	24	305-01
MRF891	5	0.62	9	24	319-04
MRF892	14	2	8.5	24	319-04
MRF894	30	6	7	24	319-04
MRF898	60	12	6.3	24	333A

**136-225 MHZ FM POWER TRANSISTORS**

Device Type	P Out Watts	P In Watts	Power Gain dB Min	V CC Volts	Package
MRF2678	15	1	12	12.5	244-04
MRF1946	30	3	10	12.5	211-07

## LOW NOISE AMPLIFIER TRANSISTORS

Device	Package	B . W Typ		Noise Figure (Max)			Gain		Max Ratings	
		FT @ GHZ	Ic mA	NF @ dB	f MHZ	IC mA	db @ Min	f MHZ	V(BR)CEO	Ic(mA)
MRF571	MACRO.X	8.0	50	2.0	1000	5.0	10.0	1000	10	70
MMBR571	SOT23	8.0	50	2.6	1000	10.0	10.5	1000	10	80
MRF2369	MACRO.X	6.0	50	2.0	1000	5.0	10.0	1000	15	70
MRF580	MACRO.X	5.0	75	2.0*	500	50.0	11.0	500	18	200
MRF581	MACRO.X	5.0	75	2.0*	500	50.0	13.0	500	18	200
BFQ19	SOT89	5.0	50	3.3	500	50.0			15	75
BFR91	MACRO.X	5.0	30	1.9*	500	2.0	16.0*	500	12	40
BFR93	SOT23	5.0	30	1.9*	500	2.0	—	—	15	35
MRF911	MACRO.X	5.0	30	2.5	1000	5.0	12.5*	1000	12	40
MMBR911	SOT23	5.0	30	2.5	1000	5.0				
MMBR930	SOT23	5.0	30	2.5*	1000	2.0	8.0*	500	12	35
BFR90	MACRO.X	5.0	14	2.4*	500	2.0	18.0*	500	15	30
BFR92	SOT23	5.0	14	2.4*	500	2.0	—	—	15	25
MRF901	MACRO.X	4.5	15	2.0	1000	5.0	10.0	1000	15	30
MMBR901	SOT23	4.5	15	1.9*	1000	5.0	16.0*	1000	15	30
MMBR920	SOT23	4.5	14	3.0*	1000	2.0	10.0*	1000	15	35
BFR96	MACRO.X	4.5	50	2.0*	500	10	12.0	500	15	100
BFQ18A	SOT89	4.0	50	—	—	—	—	—	15	150
MRF559	MACRO.X	3.0	100	—	—	—	13.0	512	18	150
MRF931	MACRO.X	3.0	1.0	3.8*	500	0.25	16.0*	500	5	5
MMBR931	SOT23	3.0	1.0	3.8*	500	0.25	10.0*	1000	5	5
MXR5943	SOT89	2.0	100	—	—	—	—	—	30	400
BFS17	SOT23	1.5	25	—	—	—	—	—	15	25
MMBR2060	SOT23	1.5	25	3.5	450	1.5	12.5	450	14	50
BFQ17	SOT89	1.2	150	—	—	—	—	—	25	300
MMBR5031	SOT23	1.0	5	2.5	450	1.0	14.0	450	10	20

\* Typ

## FIELD EFFECT TRANSISTORS

Device	Package	Re	YFs	Noise Figure (Max)		I <sub>DSS</sub> @ V <sub>DSS</sub> =15V		Max Ratings	
		mm ho @ Min	f (MHZ)	dB Max	@ f (MHZ)	Min	Max	V(BR)GSS	I <sub>B</sub> Max (mA)
2N5484	TO92	2.5	100	3.0	100	1.0	5.0	25	30
MMBF5484	SOT23	2.5	100	3.0	100	1.0	5.0	25	30
2N5486	TO92	3.5	400	3.5	400	8.0	20.0	25	30
MMBF5486	SOT23	3.5	400	3.5	400	8.0	20.0	25	30
MMBF4416	SOT23	4.0	400	4.0	400	5.0	15.0	30	20
U310	TO52	10	1kHz	3.0*	450	24†	60†	25	100
MMBFU310	SOT23	10	1kHz	3.0*	450	24†	60†	25	100
3N204	TO72	10	1kHz	5.0	450	6.0	30	30	50

\* Typ

† Measured @ V<sub>DS</sub> = 10V



## TUNING DIODES

Device*	Package	Nominal CAP ± 10% (pF) @ $V_R=4V$ F=1 MHZ		CAP Ratio Min C2/C20		Q Typ @ 4V/50 MHZ		Max Rating V(BR) R
MMBV2097	SOT23	1.0		2.0		400		30V
MMBV2098	SOT23	2.2		2.0		400		30V
MMBV2101	SOT23	6.8		2.5		400		30V
MMBV2102	SOT23	8.2		2.5		350		30V
MMBV2103	SOT23	10		2.5		350		30V
MMBV2104	SOT23	12		2.5		350		30V
MMBV2105	SOT23	15		2.5		350		30V
MMBV2106	SOT23	18		2.5		300		30V
MMBV2107	SOT23	22		2.5		300		30V
MMBV2108	SOT23	27		2.5		250		30V
MMBV2109	SOT23	33		2.5		250		30V

These Diodes exist also in TO92 (2 leads) Package

## HYPER ABRUPT DIODES UHF/VHF

Device	Package	Capacitance (pF)		(pF) @ $V_R(V)$	Cap Ratio Min C3/C25	Q Typ @ 3V/50 MHZ		Max Rating V(BR)R
		Min	Max					
MMBV105G	SOT23	1.8	2.8	25	4	350		30V
MMBV3102	SOT23	20	25	3	4.5	300		30V
MMBV109	SOT23	26	32	3	5	250		30V
MV209	TO92	26	32	3	5	250		30V

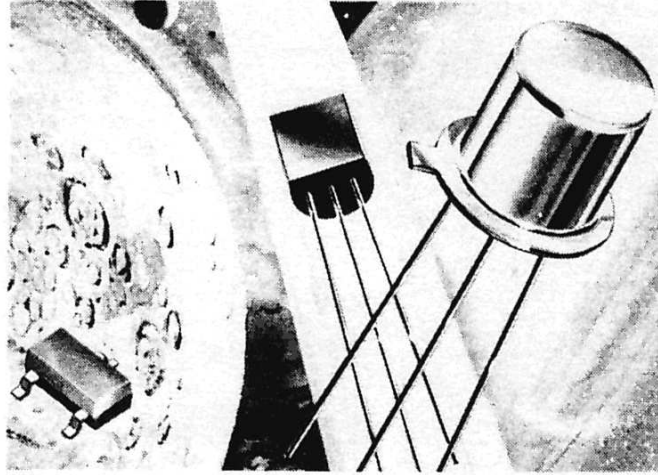
## SCHOTTKY DIODES

Device	Package	Capacitance (pF)		$V_F$ Max (Volts)		Max Rating V(BR)R
		pF Max	@ $V_R$ (Volts)	@ $I_F = 10$ mA		
MBD101	TO92	1	0	0.6		4V
MMBD101	SOT23	1	0	0.6		4V
MMBD352	SOT23	1	0	0.6		4V
MBD301	TO92	1.5	15	0.6		30V
MMBD301	SOT23	1.5	15	0.6		30V
MBD701	TO92	1	20	1.2		70V
MMBD701	SOT23	1	20	1.2		70V

## PIN DIODES

Device	Package	Capacitance		Resistance Ohms Max @ $I_F=10$ mA/100 MHZ	Max Rating V(BR)R
		pF (Max)	@ $V_R$ (Volts)		
MPN3404	TO92	2	20	0.85	20
MMBV3401	SOT23	1	20	0.70	35
MMBV3700	SOT23	1	15	0.40	200

## Package Outline Dimensions



4

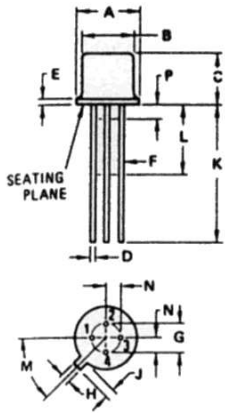
The following pages contain information on the various packages referenced on the individual data sheets. Information includes: a picture of the package, dimensions in both millimeters and inches, the various pinout configurations (styles), a cross reference for Case numbers, "old" JEDEC "TO" numbers, and the new JEDEC "TO" designation.

An information on Tape and Reel packaging capabilities is also given.

# Package Outline Dimensions

Dimensions are in inches unless otherwise noted.

## CASE 20-03 TO-72 (TO-206AF)

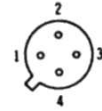


DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	5.31	5.84	0.209	0.230
B	4.52	4.95	0.178	0.195
C	4.32	5.33	0.170	0.210
D	0.41	0.53	0.016	0.021
E	-	0.76	-	0.030
F	0.41	0.48	0.016	0.019
G	2.54 BSC	0.100 BSC		
H	0.91	1.17	0.036	0.046
J	0.71	1.22	0.028	0.048
K	12.70	-	0.500	-
L	6.35	-	0.250	-
M	45° BSC	45° BSC		
N	1.27 BSC	0.050 BSC		
P	-	1.27	-	0.050

ALL JEDEC dimensions and notes apply

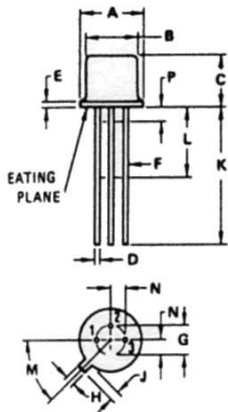


## CASE 20 STYLES



- |   |  |  |
|---|--|--|
| <p><b>STYLE 1</b><br/>PIN 1. SOURCE<br/>2. DRAIN<br/>3. GATE<br/>4. CASE LEAD</p> <p><b>STYLE 2</b><br/>PIN 1. SOURCE<br/>2. GATE<br/>3. DRAIN<br/>4. SUBSTRATE AND CASE LEAD</p> <p><b>STYLE 3</b><br/>PIN 1. DRAIN<br/>2. SOURCE<br/>3. GATE<br/>4. CASE LEAD</p> <p><b>STYLE 4</b><br/>PIN 1. SOURCE<br/>2. GATE<br/>3. DRAIN<br/>4. GATE 2 - SUBSTRATE AND CASE</p> | <p><b>STYLE 5</b><br/>PIN 1. SOURCE<br/>2. GATE 1<br/>3. DRAIN<br/>4. CASE</p> <p><b>STYLE 6</b><br/>PIN 1. DRAIN<br/>2. SOURCE AND SUBSTRATE<br/>3. GATE<br/>4. SOURCE AND SUBSTRATE</p> <p><b>STYLE 7</b><br/>PIN 1. DRAIN<br/>2. SOURCE<br/>3. GATE<br/>4. CASE AND SUBSTRATE</p> <p><b>STYLE 8</b><br/>PIN 1. EMITTER 2<br/>2. BASE 1<br/>3. COLLECTOR<br/>4. EMITTER 1<br/>BASE 2</p> | <p><b>STYLE 9</b><br/>PIN 1. DRAIN<br/>2. GATE 2<br/>3. GATE 1<br/>4. SOURCE, SUBSTRATE AND CASE</p> <p><b>STYLE 10</b><br/>PIN 1. EMITTER<br/>2. BASE<br/>3. COLLECTOR<br/>4. CASE</p> <p><b>STYLE 11</b><br/>PIN 1. EMITTER<br/>2. CATHODE<br/>3. COLLECTOR<br/>4. ANODE</p> <p><b>NOTE:</b><br/>1. ALL RULES AND NOTES WITH TO-72 OUTLINE SHALL APPLY</p> |
|---|--|--|

## CASE 22-03 TO-18 (TO-206AA)



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	5.31	5.84	0.209	0.230
B	4.52	4.95	0.178	0.195
C	4.32	5.33	0.170	0.210
D	0.406	0.533	0.016	0.021
E	-	0.762	-	0.030
F	0.406	0.483	0.016	0.019
G	2.54 BSC	0.100 BSC		
H	0.914	1.17	0.036	0.046
J	0.711	1.22	0.028	0.048
K	12.70	-	0.500	-
L	6.35	-	0.250	-
M	45° BSC	45° BSC		
N	1.27 BSC	0.050 BSC		
P	-	1.27	-	0.050

All JEDEC notes and dimensions apply.

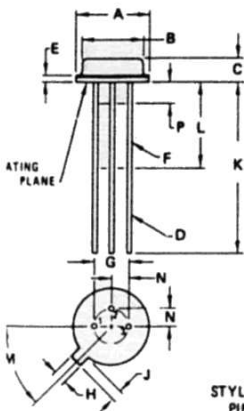


## CASE 22 STYLES



- |  |   |
|--|---|
| <p><b>STYLE 1</b><br/>PIN 1. EMITTER<br/>2. BASE<br/>3. COLLECTOR</p> <p><b>STYLE 2</b><br/>PIN 1. SOURCE, SUBSTRATE AND CASE<br/>2. GATE<br/>3. DRAIN</p> <p><b>STYLE 3</b><br/>PIN 1. SOURCE<br/>2. DRAIN<br/>3. GATE</p> <p><b>STYLE 4</b><br/>PIN 1. SOURCE<br/>2. DRAIN<br/>3. GATE &amp; CASE</p> <p><b>STYLE 5</b><br/>PIN 1. EMITTER<br/>2. BASE 1<br/>3. BASE 2</p> <p><b>STYLE 6</b><br/>PIN 1. CATHODE<br/>2. GATE<br/>3. ANODE</p> | <p><b>STYLE 7</b><br/>PIN 1. ANODE<br/>2. BASE<br/>3. CATHODE</p> <p><b>STYLE 8</b><br/>PIN 1. GATE<br/>2. ANODE 1<br/>3. ANODE 2</p> <p><b>STYLE 9</b><br/>PIN 1. ANODE 2<br/>2. ANODE 1<br/>3. GATE (CONNECTED TO CASE)</p> <p><b>STYLE 10</b><br/>PIN 1. BASE<br/>2. EMITTER<br/>3. BASE</p> <p><b>STYLE 11</b><br/>PIN 1. DRAIN<br/>2. GATE<br/>3. SOURCE, SUBSTRATE</p> <p><b>STYLE 12</b><br/>PIN 1. SOURCE<br/>2. GATE<br/>3. DRAIN (CASE)</p> |
|--|---|

## CASE 26-03 TO-46 (TO-206AB)

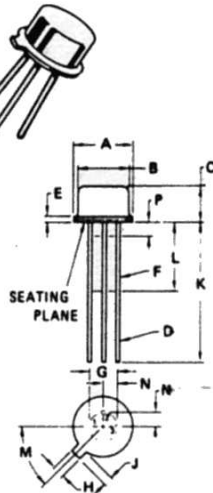


DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	5.31	5.84	0.209	0.230
B	4.52	4.95	0.178	0.195
C	1.65	2.16	0.065	0.085
D	0.406	0.533	0.016	0.021
E	-	1.02	-	0.040
F	0.305	0.483	0.012	0.019
G	2.54 BSC	0.100 BSC		
H	0.914	1.17	0.036	0.046
J	0.711	1.22	0.028	0.048
K	12.70	-	0.500	-
L	6.35	-	0.250	-
M	45° BSC	45° BSC		
N	1.27 BSC	0.050 BSC		
P	-	1.27	-	0.050

All JEDEC dimensions and notes apply



## CASE 27-02 TO-52 (TO-206AC)



- |   |  |
|---|--|
| <p><b>STYLE 1:</b><br/>PIN 1. EMITTER<br/>2. BASE<br/>3. COLLECTOR</p> <p><b>STYLE 2:</b><br/>PIN 1. DRAIN<br/>2. SOURCE<br/>3. GATE &amp; CASE</p> | <p><b>STYLE 3:</b><br/>PIN 1. EMITTER<br/>2. BASE<br/>3. BASE 2</p> <p><b>STYLE 4:</b><br/>PIN 1. SOURCE<br/>2. DRAIN<br/>3. GATE &amp; CASE</p> |
|---|--|

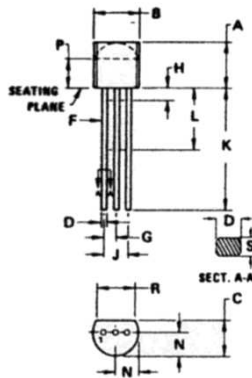
DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	5.31	5.84	0.209	0.230
B	4.52	4.95	0.178	0.195
C	2.92	3.81	0.115	0.150
D	-	0.533	-	0.021
E	-	0.762	-	0.030
F	0.406	0.483	0.016	0.019
G	2.54 BSC	0.100 BSC		
H	0.914	1.17	0.036	0.046
J	0.711	1.22	0.028	0.048
K	12.70	-	0.500	-
L	6.35	-	0.250	-
M	45° BSC	45° BSC		
N	1.27 BSC	0.050 BSC		
P	-	1.27	-	0.050

All JEDEC dimensions and notes apply

- STYLE 1:**  
PIN 1. EMITTER  
2. BASE  
3. COLLECTOR

**PACKAGE OUTLINE DIMENSIONS (continued)**

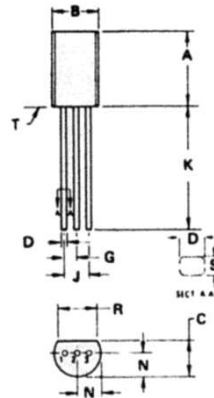
**CASE 29-02 TO-92 (TO-226AA)**



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	4.32	5.33	0.170	0.210
B	4.44	5.21	0.175	0.205
C	3.18	4.19	0.125	0.165
D	0.41	0.56	0.016	0.022
F	0.41	0.48	0.016	0.019
G	1.14	1.40	0.045	0.055
H	-	2.54	-	0.100
J	2.41	2.67	0.095	0.105
K	12.70	-	0.500	-
L	6.35	-	0.250	-
N	2.03	2.67	0.080	0.105
P	2.92	-	0.115	-
R	3.43	-	0.135	-
S	0.36	0.41	0.014	0.016

All JEDEC dimensions and notes apply.

**CASE 29-03 TO-226AE**



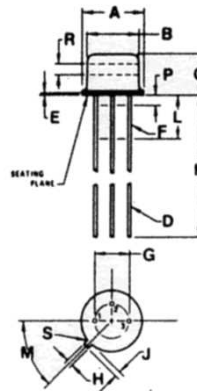
- NOTES:  
 1. DIMENSIONS A AND B ARE DATUMS.  
 2. T- IS SEATING PLANE.  
 3. POSITIONAL TOLERANCE FOR LEADS:  
 $\pm 0.10 (0.004) \text{ (M)} \text{ (A)} \text{ (B)} \text{ (C)}$   
 4. DIMENSIONING AND TOLERANCING PER ANSI Y14.5, 1973.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	7.37	7.87	0.290	0.310
B	4.44	5.21	0.175	0.205
C	3.18	4.19	0.125	0.165
D	0.46	0.61	0.018	0.024
G	1.27 BSC	-	0.050 BSC	-
J	2.54 BSC	-	0.100 BSC	-
K	12.70	-	0.500	-
N	2.03	2.92	0.080	0.115
R	3.43	-	0.135	-
S	0.46	0.61	0.018	0.024

**CASE 29 STYLES**

- |   |   |   |  |
|---|---|---|--|
| <p><b>STYLE 1:</b><br/>PIN 1. EMITTER<br/>2. BASE<br/>3. COLLECTOR</p> <p><b>STYLE 2:</b><br/>PIN 1. BASE<br/>2. EMITTER<br/>3. COLLECTOR</p> <p><b>STYLE 3:</b><br/>PIN 1. ANODE<br/>2. ANODE<br/>3. CATHODE</p> <p><b>STYLE 4:</b><br/>PIN 1. CATHODE<br/>2. CATHODE<br/>3. ANODE</p> <p><b>STYLE 5:</b><br/>PIN 1. DRAIN<br/>2. SOURCE<br/>3. GATE</p> <p><b>STYLE 6:</b><br/>PIN 1. GATE<br/>2. SOURCE &amp; SUBSTRATE<br/>3. DRAIN</p> <p><b>STYLE 7:</b><br/>PIN 1. SOURCE<br/>2. DRAIN<br/>3. GATE</p> <p><b>STYLE 8:</b><br/>PIN 1. DRAIN<br/>2. GATE<br/>3. SOURCE &amp; SUBSTRATE</p> | <p><b>STYLE 9:</b><br/>PIN 1. BASE 1<br/>2. EMITTER<br/>3. BASE 2</p> <p><b>STYLE 10:</b><br/>PIN 1. CATHODE<br/>2. GATE<br/>3. ANODE</p> <p><b>STYLE 11:</b><br/>PIN 1. ANODE<br/>2. CATHODE &amp; ANODE<br/>3. CATHODE</p> <p><b>STYLE 12:</b><br/>PIN 1. MAIN TERMINAL 1<br/>2. GATE<br/>3. MAIN TERMINAL 2</p> <p><b>STYLE 13:</b><br/>PIN 1. ANODE 1<br/>2. GATE<br/>3. CATHODE 2</p> <p><b>STYLE 14:</b><br/>PIN 1. EMITTER<br/>2. COLLECTOR<br/>3. BASE</p> <p><b>STYLE 15:</b><br/>PIN 1. ANODE 1<br/>2. CATHODE<br/>3. ANODE 2</p> | <p><b>STYLE 16:</b><br/>PIN 1. ANODE<br/>2. GATE<br/>3. CATHODE</p> <p><b>STYLE 17:</b><br/>PIN 1. COLLECTOR<br/>2. BASE<br/>3. EMITTER</p> <p><b>STYLE 18:</b><br/>PIN 1. ANODE<br/>2. CATHODE<br/>3. NOT CONNECTED</p> <p><b>STYLE 19:</b><br/>PIN 1. GATE<br/>2. ANODE<br/>3. CATHODE</p> <p><b>STYLE 20:</b><br/>PIN 1. NOT CONNECTED<br/>2. CATHODE<br/>3. ANODE</p> <p><b>STYLE 21:</b><br/>PIN 1. COLLECTOR<br/>2. EMITTER<br/>3. BASE</p> <p><b>STYLE 22:</b><br/>PIN 1. SOURCE<br/>2. GATE<br/>3. DRAIN</p> <p><b>STYLE 23:</b><br/>PIN 1. GATE<br/>2. SOURCE<br/>3. DRAIN</p> | <p><b>STYLE 24:</b><br/>1. EMITTER<br/>2. COLLECTOR/ANODE<br/>3. CATHODE</p> <p><b>STYLE 25:</b><br/>1. MT 1<br/>2. GATE<br/>3. MT 2</p> <p><b>STYLE 26:</b><br/>PIN 1. VCC<br/>2. GROUND 2<br/>3. OUTPUT</p> <p><b>STYLE 27:</b><br/>PIN 1. MT<br/>2. SUBSTRATE<br/>3. MT</p> <p><b>STYLE 28:</b><br/>PIN 1. CATHODE<br/>2. ANODE<br/>3. GATE</p> <p><b>STYLE 29:</b><br/>PIN 1. NOT CONNECTED<br/>2. ANODE<br/>3. CATHODE</p> <p><b>STYLE 30:</b><br/>PIN 1. DRAIN<br/>2. GATE<br/>3. SOURCE</p> |
|---|---|---|--|

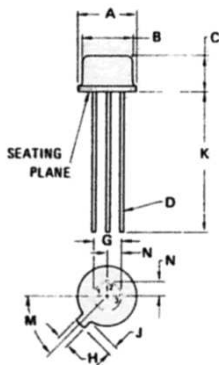
**CASE 31-03 TO-5 (TO-205AA)**



- STYLE 1:**  
PIN 1. EMITTER  
2. BASE  
3. COLLECTOR
- STYLE 2:**  
PIN 1. CATHODE  
2. GATE  
3. ANODE
- STYLE 3:**  
PIN 1. GATE  
2. CATHODE  
3. ANODE

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	8.51	9.40	0.335	0.370
B	7.75	8.51	0.305	0.335
C	6.10	6.60	0.240	0.260
D	0.406	0.533	0.016	0.021
E	0.229	3.18	0.009	0.125
F	0.406	0.483	0.016	0.019
G	5.08 BSC	-	0.200 BSC	-
H	0.711	0.864	0.028	0.034
J	0.734	1.14	0.029	0.045
K	38.10	44.45	1.500	1.750
L	6.35	-	0.250	-
M	45° BSC	-	45° BSC	-
N	-	-	-	-
P	-	1.27	-	0.050
R	2.54	-	0.100	-
S	-	0.25	-	0.010

**CASE 31A-01**

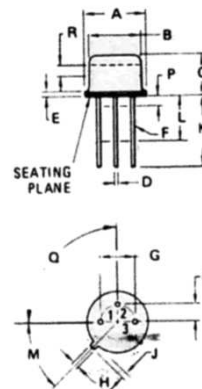


- STYLE 1:**  
PIN 1. EMITTER  
2. BASE  
3. COLLECTOR
- STYLE 2:**  
PIN 1. INPUT  
2. OUTPUT  
3. GROUND

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	8.51	9.40	0.335	0.370
B	7.75	8.51	0.305	0.335
C	3.81	4.57	0.150	0.180
D	0.41	0.48	0.016	0.019
G	5.08 BSC	-	0.200 BSC	-
H	0.71	0.86	0.028	0.034
J	0.74	1.14	0.029	0.045
K	12.70	-	0.500	-
M	45° BSC	-	45° BSC	-
N	2.54 BSC	-	0.100 BSC	-

NOTE:  
 1. LEADS WITHIN 0.36 mm (0.014) DIA OF TRUE POSITION AT SEATING PLANE AT MAXIMUM MATERIAL CONDITION.

**CASE 79-02 TO-39 (TO-205AD)**

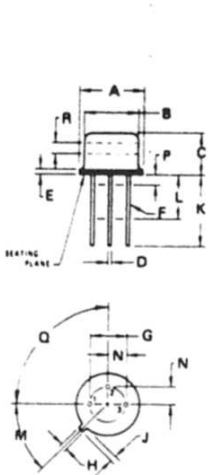


DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	8.89	9.40	0.350	0.370
B	8.00	8.51	0.315	0.335
C	6.10	6.60	0.240	0.260
D	0.406	0.533	0.016	0.021
E	0.229	3.18	0.009	0.125
F	0.406	0.483	0.016	0.019
G	4.83	5.33	0.190	0.210
H	0.711	0.864	0.028	0.034
J	0.737	1.02	0.029	0.040
K	12.70	-	0.500	-
L	6.35	-	0.250	-
M	45° NOM	-	45° NOM	-
P	-	1.27	-	0.050
Q	90° NOM	-	90° NOM	-
R	2.54	-	0.100	-

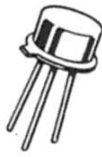
All JEDEC dimensions and notes apply.

# PACKAGE OUTLINE DIMENSIONS (continued)

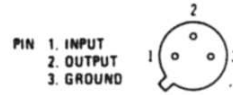
## CASE 79-03



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	9.02	9.30	0.355	0.366
B	8.00	8.51	0.315	0.335
C	4.19	4.57	0.165	0.180
D	0.43	0.53	0.017	0.021
E	0.43	0.89	0.017	0.035
F	0.41	0.48	0.016	0.019
G	4.83	5.33	0.190	0.210
H	0.71	0.86	0.028	0.034
J	0.74	1.02	0.029	0.040
K	12.70	-	0.500	-
M	45° NOM	-	45° NOM	-
N	2.54 TYP	-	0.100 TYP	-
Q	90° NOM	-	90° NOM	-



## CASE 79 STYLES



STYLE 1:  
PIN 1. EMITTER  
2. BASE  
3. COLLECTOR

STYLE 4:  
PIN 1. MAIN TERM 1  
2. GATE  
3. MAIN TERM 2

STYLE 2:  
PIN 1. DRAIN  
2. SOURCE  
3. GATE

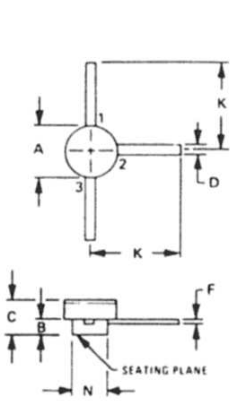
STYLE 5:  
PIN 1. COLLECTOR  
2. BASE  
3. EMITTER

STYLE 3:  
PIN 1. CATHODE  
2. GATE  
3. ANODE

STYLE 6:  
PIN 1. SOURCE  
2. GATE  
3. DRAIN  
(CASE)

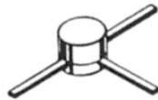
NOTES:  
1. ALL RULES AND NOTES ASSOCIATED WITH TO 39 OUTLINE SHALL APPLY.

## CASE 176-02

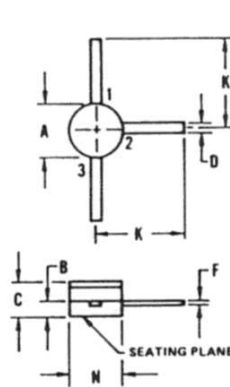


NOTE:  
A Tolerance of .25 mm (0.010) must be allowed at point leads protrude from package for glass run over.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	2.03	2.67	0.080	0.105
B	0.38	0.76	0.015	0.030
C	1.27	2.03	0.050	0.080
D	0.25	0.41	0.010	0.016
F	0.08	0.15	0.003	0.006
K	4.06	4.57	0.160	0.180
N	1.47	1.78	0.058	0.070



## CASE 176B-01



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	2.03	2.67	0.080	0.105
B	0.38	0.76	0.015	0.030
C	1.27	2.03	0.050	0.080
D	0.25	0.41	0.010	0.016
F	0.08	0.15	0.003	0.006
K	4.06	4.57	0.160	0.180
N	2.03	2.67	0.080	0.105



## CASE 176 STYLES

STYLE 1:  
PIN 1. BASE  
2. EMITTER  
3. COLLECTOR

STYLE 2:  
PIN 1. SOURCE  
2. GATE  
3. DRAIN

STYLE 3:  
PIN 1. DRAIN  
2. SOURCE  
3. GATE

STYLE 4:  
PIN 1. ANODE 2  
2. ANODE 1  
3. CATHODE

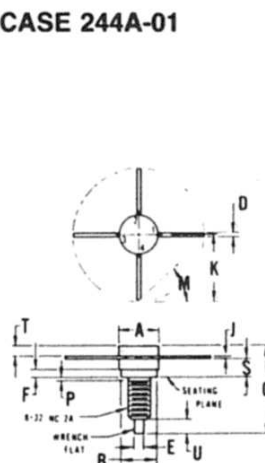
STYLE 5:  
PIN 1. CATHODE  
2. NOT CONNECTED  
3. ANODE

STYLE 6:  
PIN 1. CATHODE  
2. ANODE  
3. ANODE

STYLE 7:  
PIN 1. EMITTER  
2. BASE  
3. COLLECTOR

STYLE 8:  
PIN 1. ANODE  
2. NC  
3. CATHODE

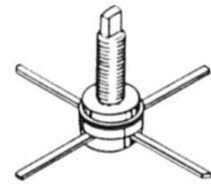
## CASE 244A-01



STYLE 1:  
PIN 1. EMITTER  
2. BASE  
3. EMITTER  
4. COLLECTOR

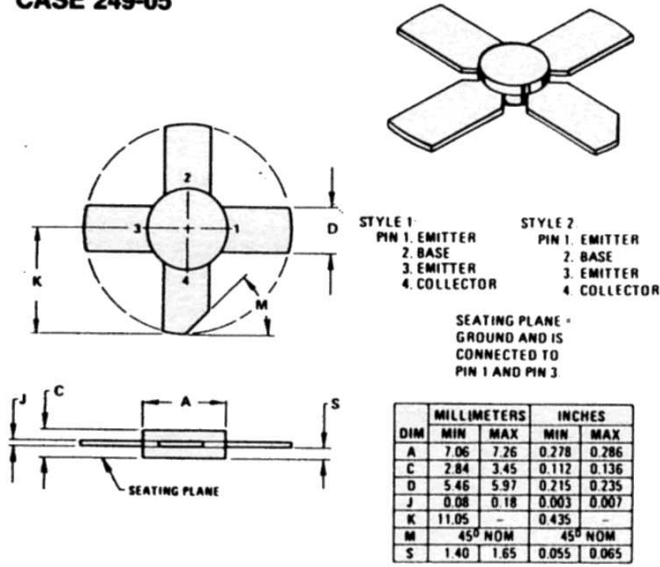
STYLE 2:  
PIN 1. COMMON  
2. OUTPUT  
3. COMMON  
4. INPUT

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	7.06	7.26	0.278	0.286
B	6.20	6.50	0.244	0.256
C	15.24	16.51	0.600	0.650
D	0.66	0.86	0.026	0.034
E	1.40	1.65	0.055	0.065
F	1.52	-	0.060	-
J	0.10	0.15	0.004	0.006
K	11.17	-	0.440	-
M	45° NOM	-	45° NOM	-
P	-	1.27	-	0.050
S	2.74	3.35	0.108	0.132
T	1.40	1.78	0.055	0.070
U	2.92	3.68	0.115	0.145

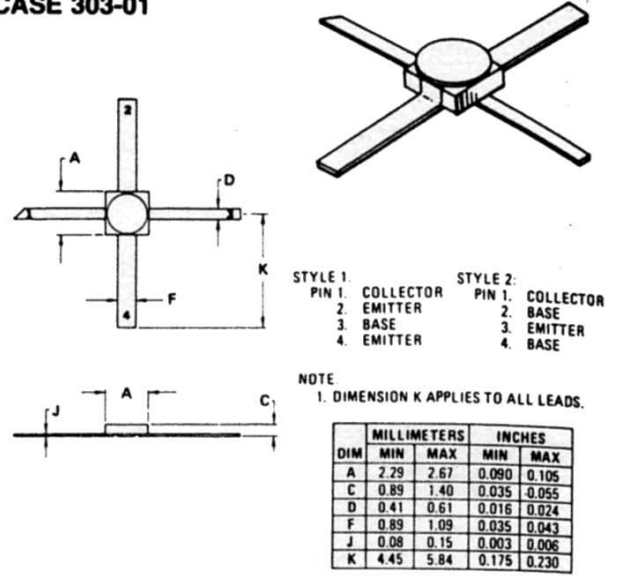


**PACKAGE OUTLINE DIMENSIONS (continued)**

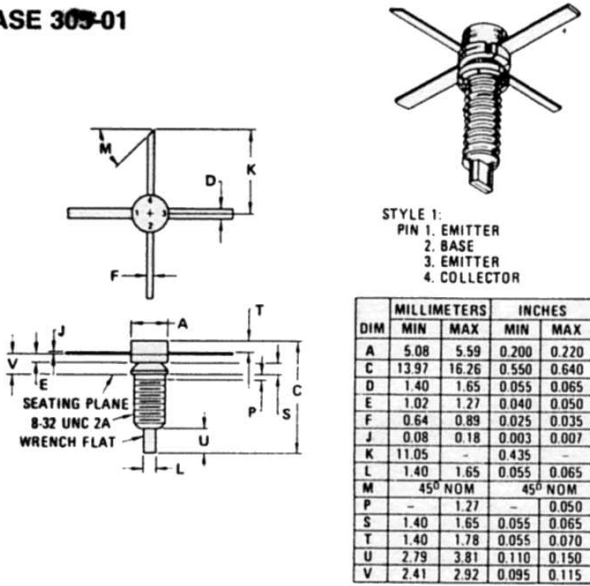
**CASE 249-05**



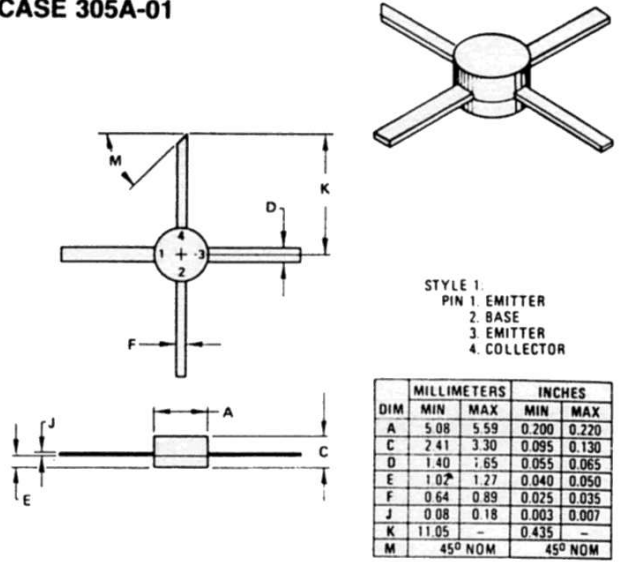
**CASE 303-01**



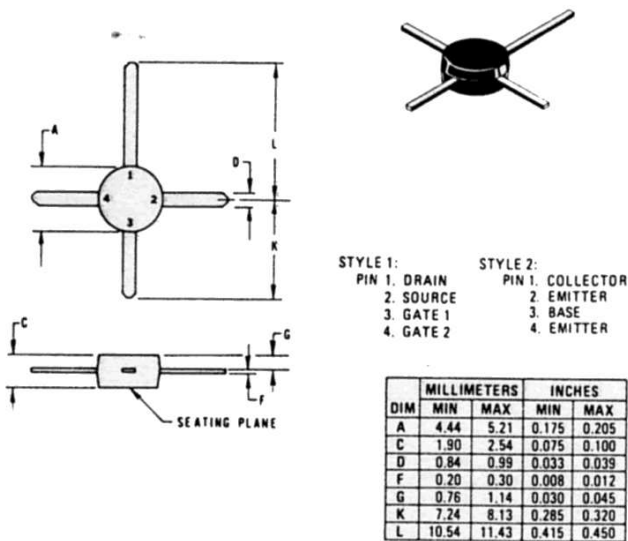
**CASE 305-01**



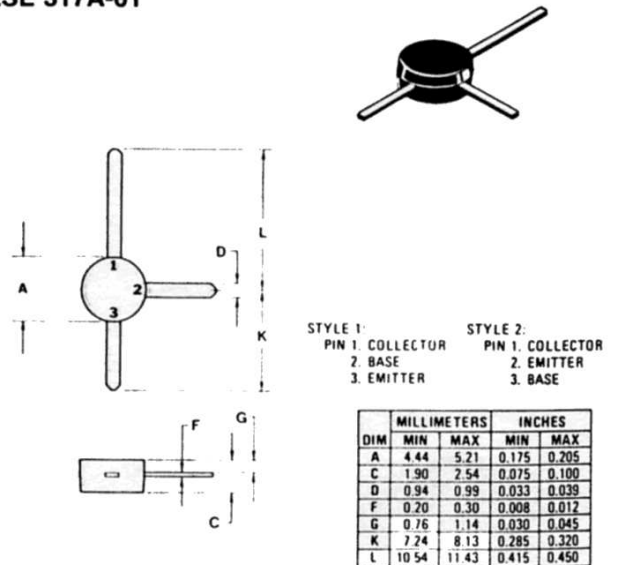
**CASE 305A-01**



**CASE 317-01**



**CASE 317A-01**

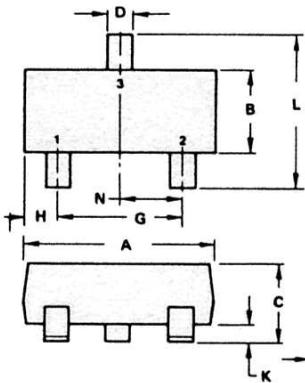


4



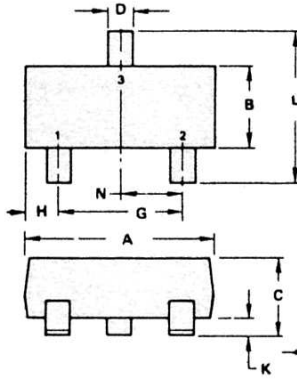
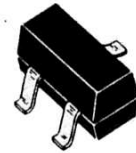
# PACKAGE OUTLINE DIMENSIONS (continued)

## CASE 318 TO-236AA



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	2.80	3.04	0.1102	0.1197
B	1.20	1.40	0.0472	0.0551
C	0.85	1.20	0.033	0.0472
D	0.37	0.46	0.015	0.0177
F	0.085	0.13	0.0034	0.0051
G	1.78	2.04	0.0701	0.0807
H	0.51	0.60	0.020	0.0236
K	0.10	0.25	0.004	0.0098
L	2.10	2.50	0.083	0.0984
M	0.45	0.60	0.018	0.0236
N	0.89	1.02	0.035	0.0401

## CASE 318 TO-236AB (Low Profile)



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	2.80	3.04	0.1102	0.1197
B	1.20	1.40	0.0472	0.0551
C	0.89	1.04	0.035	0.0412
D	0.37	0.46	0.015	0.0177
F	0.085	0.13	0.0034	0.0051
G	1.78	2.04	0.0701	0.0807
H	0.51	0.60	0.020	0.0236
K	0.13	0.10	0.0005	0.0040
L	2.10	2.50	0.083	0.0984
M	0.45	0.60	0.018	0.0236
N	0.89	1.02	0.035	0.0401

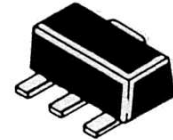
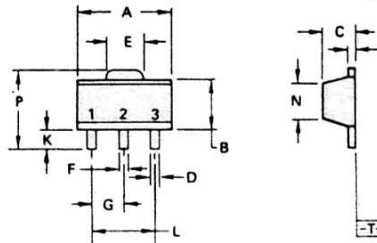
## CASE 318 STYLES

- |   |  |  |
|---|--|--|
| <p><b>STYLE 6:</b><br/>PIN 1. BASE<br/>2. EMITTER<br/>3. COLLECTOR</p>      | <p><b>STYLE 10:</b><br/>PIN 1. DRAIN<br/>2. SOURCE<br/>3. GATE</p>                 | <p><b>STYLE 14:</b><br/>PIN 1. CATHODE<br/>2. GATE<br/>3. ANODE</p>          |
| <p><b>STYLE 7:</b><br/>PIN 1. EMITTER<br/>2. BASE<br/>3. COLLECTOR</p>      | <p><b>STYLE 11:</b><br/>PIN 1. ANODE<br/>2. CATHODE<br/>3. CATHODE ANODE ANODE</p> | <p><b>STYLE 15:</b><br/>PIN 1. GATE<br/>2. CATHODE<br/>3. ANODE</p>          |
| <p><b>STYLE 8:</b><br/>PIN 1. ANODE<br/>2. NO CONNECTION<br/>3. CATHODE</p> | <p><b>STYLE 12:</b><br/>PIN 1. CATHODE<br/>2. CATHODE<br/>3. ANODE</p>             | <p><b>STYLE 16:</b><br/>PIN 1. ANODE<br/>2. CATHODE<br/>3. CATHODE</p>       |
| <p><b>STYLE 9:</b><br/>PIN 1. ANODE<br/>2. ANODE<br/>3. CATHODE</p>         | <p><b>STYLE 13:</b><br/>PIN 1. SOURCE<br/>2. DRAIN<br/>3. GATE</p>                 | <p><b>STYLE 17:</b><br/>PIN 1. NO CONNECTION<br/>2. ANODE<br/>3. CATHODE</p> |

STYLES 1 THRU 5 ARE OBSOLETE.

**NOTES**  
1. 318-02 MEETS ALL JEDEC DIMENSIONAL REQUIREMENTS FOR TO-236AA.

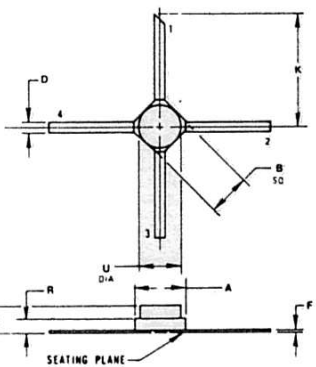
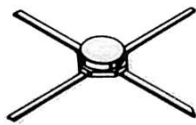
## CASE 345-01



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	4.40	4.60	0.174	0.181
B	2.29	2.60	0.091	0.102
C	1.40	1.60	0.056	0.062
D	0.36	0.48	0.015	0.018
E	1.62	1.80	0.064	0.070
F	0.44	0.53	0.018	0.020
G	1.50 BSC		0.059 BSC	
J	0.35	0.44	0.014	0.017
K	0.80	1.04	0.032	0.040
L	3.00 BSC		0.118 BSC	
N	2.04	2.28	0.081	0.089
P	3.94	4.25	0.156	0.167

- |   |  |
|---|--|
| <p><b>STYLE 1:</b><br/>PIN 1. BASE<br/>2. COLLECTOR<br/>3. EMITTER</p>      | <p><b>STYLE 3:</b><br/>PIN 1. GATE<br/>2. ANODE<br/>3. CATHODE</p> |
| <p><b>STYLE 2:</b><br/>PIN 1. ANODE<br/>2. CATHODE<br/>3. NO CONNECTION</p> | <p><b>STYLE 4:</b><br/>PIN 1. DRAIN<br/>2. GATE<br/>3. SOURCE</p>  |

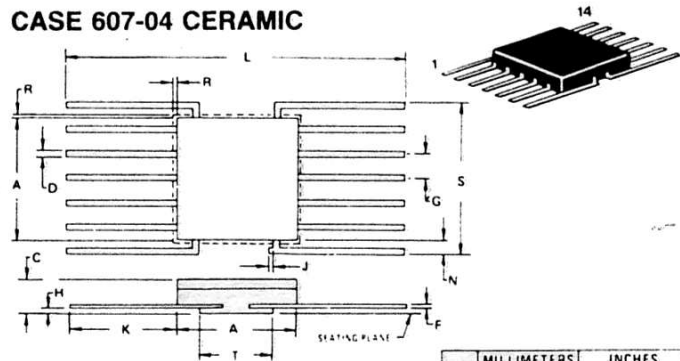
## CASE 358-01



- |   |   |
|---|---|
| <p><b>STYLE 1:</b><br/>PIN 1. BASE<br/>2. EMITTER<br/>3. COLLECTOR<br/>4. EMITTER</p> | <p><b>STYLE 2:</b><br/>PIN 1. DRAIN<br/>2. SOURCE<br/>3. GATE 1<br/>4. GATE 2</p> |
|---|---|

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	2.41	2.92	0.095	0.115
B	1.95	2.36	0.077	0.093
C	1.09	1.60	0.043	0.063
D	0.43	0.58	0.017	0.023
F	0.07	0.15	0.003	0.006
K	4.82	6.60	0.190	0.260
R	0.53	0.96	0.021	0.038
U	1.98	2.18	0.078	0.086

## CASE 607-04 CERAMIC



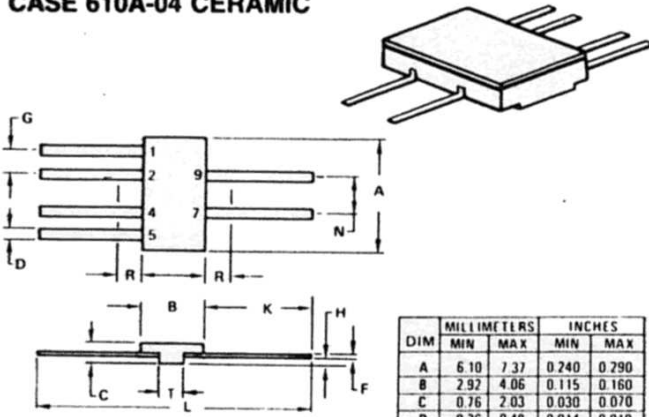
DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	6.10	6.99	0.240	0.275
C	0.76	2.03	0.030	0.070
D	0.25	0.48	0.010	0.019
F	0.08	0.15	0.003	0.006
G	1.27 BSC		0.050 BSC	
H	0.13	0.89	0.005	0.035
J	-	0.38	-	0.015
K	6.35	-	0.250	-
L	18.80	-	0.740	-
N	0.25	-	0.010	-
R	-	0.38	-	0.015
S	7.62	8.38	0.300	0.330
T	4.45	4.95	0.175	0.195

- STYLE 1**  
BASE 2, 6, 9, 13  
EMITTER 3, 5, 10, 12  
COLLECTOR 1, 7, 8, 14  
FOR COMPLEMENTARY QUADS  
NPN PINS 1 THRU 3, 12 THRU 14  
PNP PINS 5 THRU 7, 8 THRU 10  
(REFER TO STYLE 1 FOR PIN IDENTIFICATION)



# PACKAGE OUTLINE DIMENSIONS (continued)

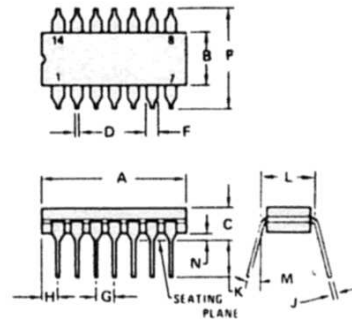
## CASE 610A-04 CERAMIC



**STYLE 1**  
 BASE 1, 5  
 EMITTER 2, 4  
 COLLECTOR 9, 7  
**FOR COMPLEMENTARY PAIRS**  
 NPN PINS 1, 2, 9  
 PNP PINS 4, 5, 7  
 (REFER TO STYLE 1 FOR PIN IDENTIFICATION)

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	6.10	7.37	0.240	0.290
B	2.92	4.06	0.115	0.160
C	0.76	2.03	0.030	0.070
D	0.36	0.48	0.014	0.019
F	0.08	0.15	0.003	0.006
G	1.27 BSC		0.050 BSC	
H	0.13	0.89	0.005	0.035
K	3.81		0.150	
L	10.54		0.415	
N	2.54 BSC		0.100 BSC	
R		1.27		0.050
T	1.65	2.03	0.065	0.080

## CASE 632-02 TO-116 CERAMIC

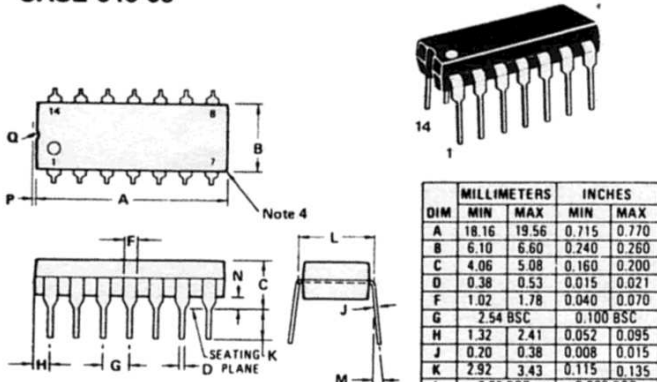


**STYLE 1**  
 COLLECTOR 1, 7, 8, 14  
 BASE 2, 6, 9, 13  
 EMITTER 3, 5, 10, 12  
**COMPLEMENTARY PAIRS**  
**TYPE 1**  
 NPN 1 THRU 3, 5 THRU 7  
 PNP 8 THRU 10, 12 THRU 14  
 (REFER TO STYLE 1 FOR PIN IDENTIFICATION)

**TYPE 2**  
 NPN 1 THRU 3, 12 THRU 14  
 PNP 5 THRU 7, 8 THRU 10

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	16.8	19.9	0.660	0.785
B	5.59	7.11	0.220	0.280
C		5.08		0.200
D	0.381	0.584	0.015	0.023
F	0.77	1.77	0.030	0.070
G	2.54 BSC		0.100 BSC	
J	0.203	0.381	0.008	0.015
K	2.54		0.100	
L	7.62 BSC		0.300 BSC	
M		15°		15°
N	0.51	0.76	0.020	0.030
P		8.25		0.325

## CASE 646-05

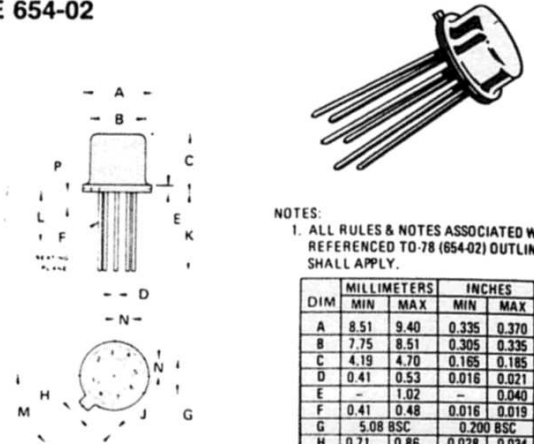


**STYLE 1**  
 BASE 2, 6, 9, 13  
 EMITTER 3, 5, 10, 12  
 COLLECTOR 1, 7, 8, 14  
**COMPLEMENTARY PAIRS**  
**TYPE 1**  
 NPN 1 THRU 3, 5 THRU 7  
 PNP 8 THRU 10, 12 THRU 14  
 (REFER TO STYLE 1 FOR PIN IDENTIFICATION)

**TYPE 2**  
 NPN 1 THRU 3, 12 THRU 14  
 PNP 5 THRU 7, 8 THRU 10

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	18.16	19.56	0.715	0.770
B	6.10	6.60	0.240	0.260
C	4.06	5.08	0.160	0.200
D	0.38	0.53	0.015	0.021
F	1.02	1.78	0.040	0.070
G	2.54 BSC		0.100 BSC	
H	1.32	2.41	0.052	0.095
J	0.20	0.38	0.008	0.015
K	2.92	3.43	0.115	0.135
L	7.62 BSC		0.300 BSC	
M	0°	10°	0°	10°
N	0.51	1.02	0.020	0.040

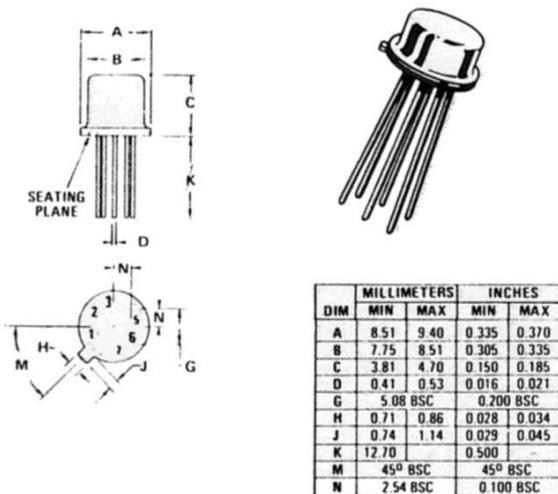
## CASE 654-02



NOTES:  
 1. ALL RULES & NOTES ASSOCIATED WITH REFERENCED TO-78 (654-02) OUTLINE SHALL APPLY.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	8.51	9.40	0.335	0.370
B	7.75	8.51	0.305	0.335
C	4.19	4.70	0.165	0.185
D	0.41	0.53	0.016	0.021
E		1.02		0.040
F	0.41	0.48	0.016	0.019
G	5.08 BSC		0.200 BSC	
H	0.71	0.86	0.028	0.034
J	0.74	1.14	0.029	0.045
K	2.70		0.500	
L	6.35		0.250	
M		45° BSC		45° BSC
N	2.54		0.100 BSC	
P		1.27		0.050

## CASE 654-07



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	8.51	9.40	0.335	0.370
B	7.75	8.51	0.305	0.335
C	3.81	4.70	0.150	0.185
D	0.41	0.53	0.016	0.021
G	5.08 BSC		0.200 BSC	
H	0.71	0.86	0.028	0.034
J	0.74	1.14	0.029	0.045
K	12.70		0.500	
M		45° BSC		45° BSC
N	2.54 BSC		0.100 BSC	

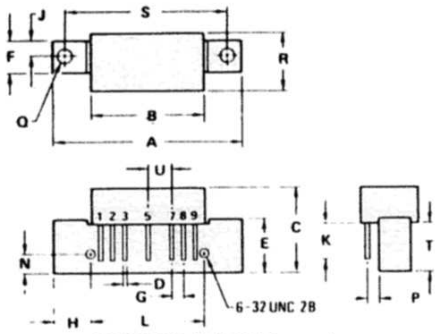
## CASE 654 STYLES

- STYLE 1:**  
 PIN 1. COLLECTOR  
 2. BASE  
 3. EMITTER  
 4. OMITTED  
 5. EMITTER  
 6. BASE  
 7. COLLECTOR  
 8. OMITTED
- STYLE 2:**  
 PIN 1. COLLECTOR  
 2. BASE  
 3. EMITTER  
 4. OMITTED  
 5. SOURCE  
 6. DRAIN  
 7. GATE  
 8. OMITTED
- STYLE 3:**  
 PIN 1. EMITTER  
 2. BASE  
 3. COLLECTOR  
 4. OMITTED  
 5. ANODE  
 6. NO CONNECTION  
 7. CATHODE  
 8. OMITTED
- STYLE 4:**  
 PIN 1. GATE  
 2. SOURCE  
 3. DRAIN  
 4. OMITTED  
 5. DRAIN  
 6. SOURCE  
 7. GATE  
 8. OMITTED
- STYLE 5:**  
 SIDE 1 (NPN)  
 PIN 1. COLLECTOR  
 2. BASE  
 3. EMITTER  
 4. OMITTED  
 SIDE 2 (PNP)  
 5. EMITTER  
 6. BASE  
 7. COLLECTOR  
 8. OMITTED
- STYLE 6:**  
 PIN 1. SOURCE  
 2. DRAIN  
 3. GATE  
 4. OMITTED  
 5. SOURCE  
 6. DRAIN  
 7. GATE  
 8. OMITTED

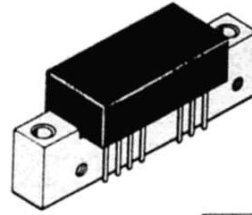


# PACKAGE OUTLINE DIMENSIONS (continued)

## CASE 714-02



FIRST STAGE: PIN 1, RF IN  
 4, RF OUT  
 SECOND STAGE: PIN 6, RF IN  
 9, RF OUT  
 V<sub>dc</sub>: PIN 5  
 DC AND RF GROUND: PINS 2, 3, 7, 8  
 NOTE  
 1 MOUNTING HOLES WITHIN  
 0.25 mm (0.010) DIA OF TRUE  
 POSITION AT MAXIMUM  
 MATERIAL CONDITION



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	-	45.08	-	1.775
B	26.42	26.92	1.040	1.060
C	20.57	21.34	0.810	0.840
D	0.46	0.56	0.018	0.022
E	11.81	12.95	0.465	0.510
F	7.62	8.13	0.300	0.320
G	2.41	2.67	0.095	0.105
H	9.65	9.78	0.380	0.385
J	3.96 BSC	-	0.156 BSC	-
K	6.86	7.37	0.270	0.290
L	25.40 BSC	-	1.000 BSC	-
N	4.06	4.32	0.160	0.170
P	2.16	2.92	0.085	0.115
Q	3.76	4.27	0.148	0.168
R	-	15.11	-	0.595
S	38.10 BSC	-	1.500 BSC	-
T	11.05	11.43	0.435	0.450
U	4.95	5.21	0.195	0.205



# **Front Page of Data Sheets of Integrated Circuits**

**Integrated Circuits**

**5**



# MC12000

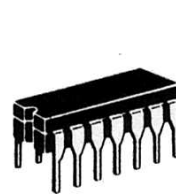
## DIGITAL MIXER/TRANSLATOR (D Flip-Flop w/Translator)

The MC12000 is intended for use as a digital mixer in phase-locked loop frequency synthesizers and other applications where a MECL "D" flip-flop with translators is required. Toggle frequency is typically 250 MHz. TTL to MECL and MECL to TTL translators are provided to facilitate interfacing with MECL or TTL circuits.

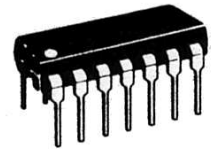
The MC12000 is designed to operate from a single power supply of either +5.0 Vdc or -5.2 Vdc.

## DIGITAL MIXER/TRANSLATOR

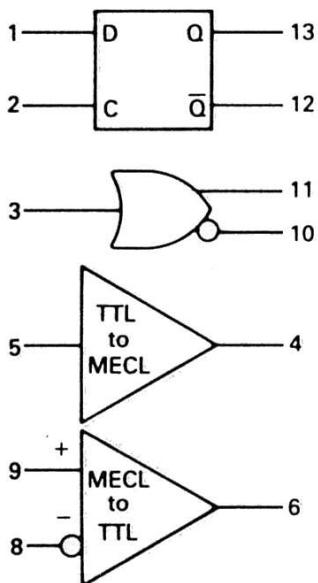
**P SUFFIX**  
PLASTIC PACKAGE  
CASE 646



**L SUFFIX**  
CERAMIC PACKAGE  
CASE 632



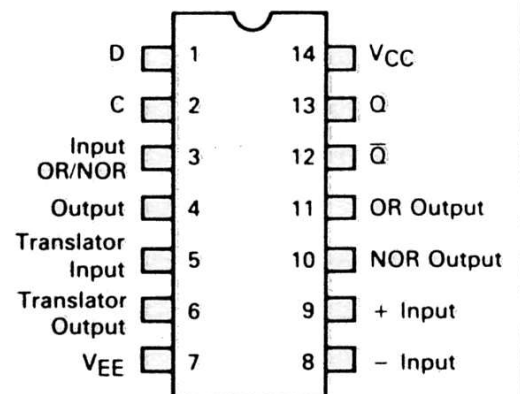
### LOGIC DIAGRAM



D	Q <sub>n</sub>	Q <sub>n+1</sub>
0	0	0
0	1	0
1	0	1
1	1	1

VCC = Pin 14  
VEE = Pin 7

### PIN ASSIGNMENT





# MOTOROLA

## MC12002/ MC12502

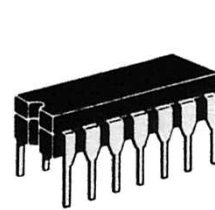
### ANALOG MIXER

The MC12002/MC12502 is a double balanced analog mixer, including an input amplifier feeding the mixer carrier port and a temperature compensated bias regulator. The input circuits for both the amplifier and mixer are differential amplifier circuits. The on-chip regulator provides all of the required biasing.

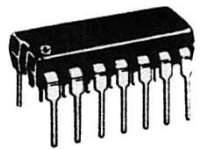
This circuit is designed for use as a balanced mixer in high-frequency wide-band circuits. Other typical applications include suppressed carrier and amplitude modulation, synchronous AM detection, FM detection, phase detection, and frequency doubling, at frequencies up to UHF.

### ANALOG MIXER

**P SUFFIX**  
PLASTIC PACKAGE  
CASE 646

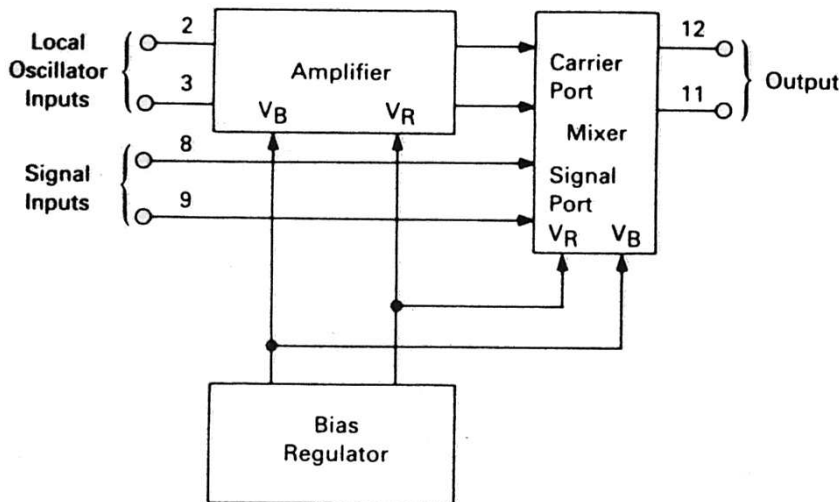


**L SUFFIX**  
CERAMIC PACKAGE  
CASE 632-02

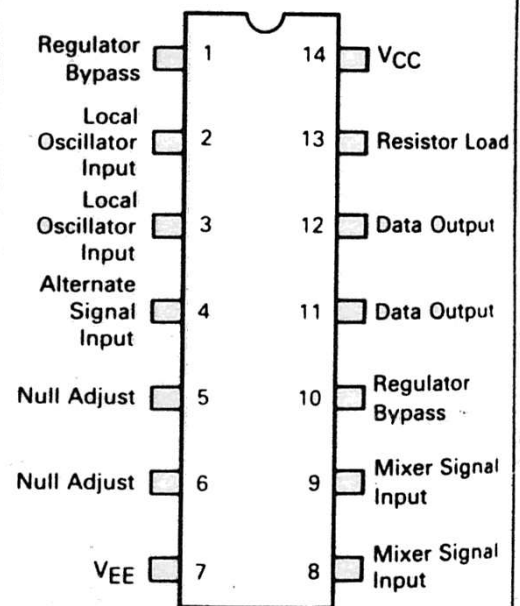


5

### LOGIC DIAGRAM



### PIN ASSIGNMENT



### TWO-MODULUS PRESCALER

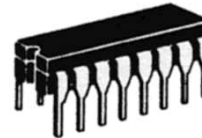
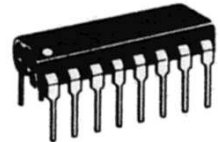
These devices are two-modulus prescalers which will divide by 5 and 6, 8 and 9, and 10 and 11, respectively. A MECL-to-TTL translator is provided to interface directly with the MC12014 Counter Control Logic. In addition, there is a buffered clock input and MECL bias voltage source. Details of operation are on the MC12012 data sheet.

- 600 MHz (Typ) Toggle Frequency
- MC12009 ( $\div 5/6$ ), MC12011 ( $\div 8/9$ ), MC12013 ( $\div 10/11$ )
- MECL to TTL Translator on Chip
- MECL and TTL Enable Inputs
- +5.0 or -5.2 V Operation\*
- Buffered Clock Input — Series Input RC Typ, 20 Ohms and 4 pF
- $V_{BB}$  Reference Voltage
- 310 Milliwatts (Typ)

\*When using +5.0 V supply, apply +5.0 V to pin 1 ( $V_{CCO}$ ), pin 6 (TTL  $V_{CC}$ ), pin 16 ( $V_{CC}$ ), and ground pin 8 ( $V_{EE}$ ). When using -5.2 V supply, ground pin 1 ( $V_{CCO}$ ), pin 6 (TTL  $V_{CC}$ ), and pin 16 ( $V_{CC}$ ) and apply -5.2 V to pin 8 ( $V_{EE}$ ). If the translator is not required, pin 6 may be left open to conserve dc power drain.

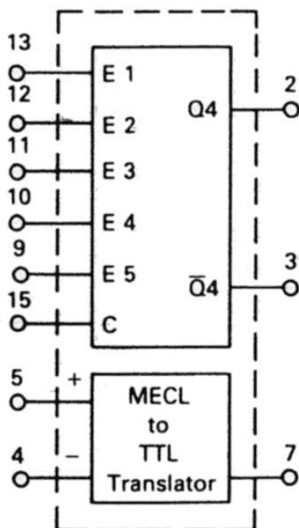
### TWO-MODULUS PRESCALER

**P SUFFIX**  
 PLASTIC PACKAGE  
 CASE 648



**L SUFFIX**  
 CERAMIC PACKAGE  
 CASE 620

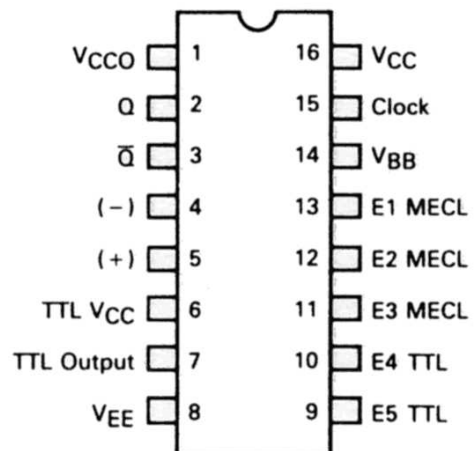
### LOGIC DIAGRAM



$V_{CCO}$  = pin 1  
 $V_{CC}$  = pin 16  
 $V_{EE}$  = pin 8

### PIN ASSIGNMENT

**5**





**MOTOROLA**

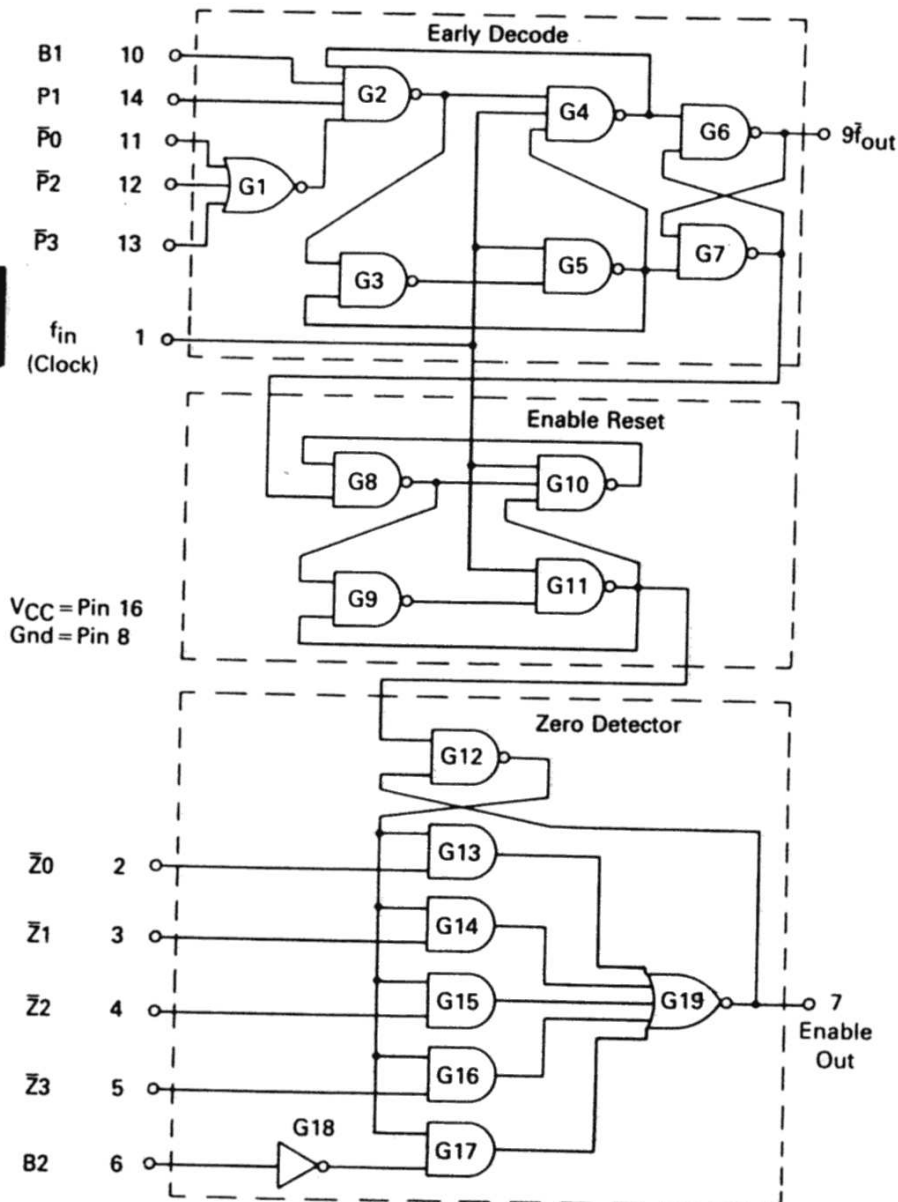
# MC12014/ MC12514

## COUNTER CONTROL LOGIC

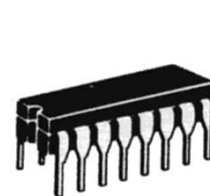
The MC12014 monolithic counter control logic unit is designed for use with the MC12013 Two-Modulus Prescaler and the MC4016 Programmable Counter to accomplish direct high-frequency programming. The MC12014 consists of a zero detector which controls the modulus of the MC12013, and an early decode function which controls the MC4016. The early decode feature also increases the useful frequency range of the MC4016 from 8.0 MHz to 25 MHz.

## COUNTER CONTROL LOGIC

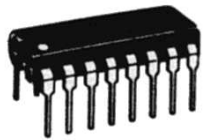
### LOGIC DIAGRAM



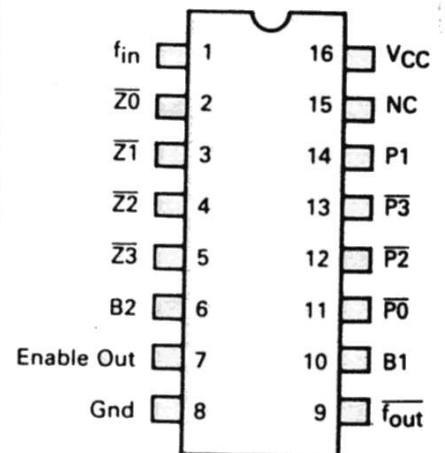
**P SUFFIX**  
PLASTIC PACKAGE  
CASE 648



**L SUFFIX**  
CERAMIC PACKAGE  
CASE 620



### PIN ASSIGNMENT





## Advance Information

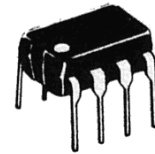
### LOW-POWER TWO-MODULUS PRESCALER

The MC12015, MC12016 and MC12017 are two-modulus prescalers which will divide by 32 and 33, 40 and 41, and 64 and 65 respectively. An internal regulator is provided to allow these devices to be used over a wide range of power-supply voltages. Regulated operation is obtained by connecting supply voltages of 4.5 to 5.5 V to both Pin 7 and Pin 8. Unregulated operation is obtained by connecting voltages greater than 5.5 to Pin 8 and leaving Pin 7 open.

- 225 MHz Toggle Frequency
- Low-Power—7.5 mA Max at 6.8 V
- Control Input and Output are Compatible with Standard CMOS
- Connecting Pins 2 and 3 Allows Driving One TTL Load
- Supply Voltage 4.5 V to 9.5 V

### MECL PLL COMPONENTS

#### LOW-POWER TWO - MODULUS PRESCALER



P SUFFIX  
PLASTIC PACKAGE  
CASE 626

### MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Regulated Voltage, Pin 7	$V_{reg}$	8.0	Vdc
Power Supply Voltage, Pin 8	$V_{CC}$	10.0	Vdc
Operating Temperature Range	$T_A$	-40 to +85	°C
Storage Temperature Range	$T_{stg}$	-65 to +175	°C

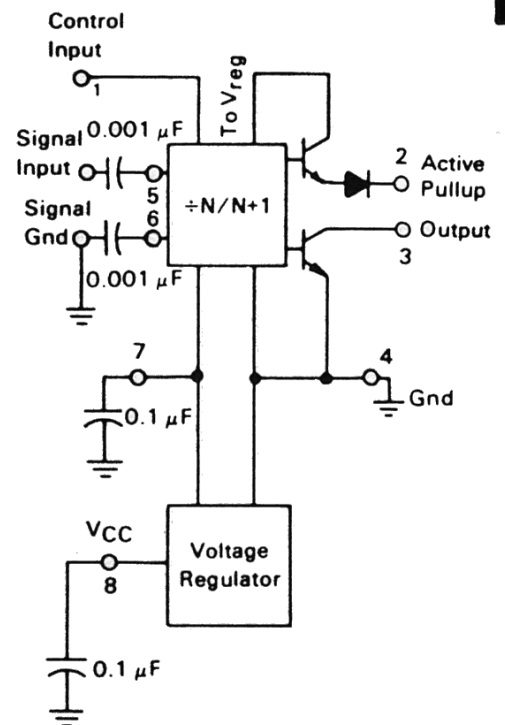
### ELECTRICAL CHARACTERISTICS ( $V_{CC} = 5.5$ to $9.5$ , $V_{reg} = 4.5$ to $5.5$ V $T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$ )

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine wave input)	$f_{max}$	225	—	—	MHz
	$f_{min}$	—	—	35	MHz
Supply Current	$I_{CC}$	—	6.0	7.8	mA
Control Input High (÷32, 40 or 64)		2.0	—	—	V
Control Input Low (÷33, 41 or 65)		—	—	0.8	V
Output Voltage High* ( $I_{source} = 50 \mu\text{A}$ )	$V_{OH}$	2.5	—	—	V
Output Voltage Low* ( $I_{sink} = 2 \text{ mA}$ )	$V_{OL}$	—	—	0.5	V
Output Voltage Sensitivity 35 MHz	$V_{in}$	400	—	800	mVPP
50-255 MHz		200	—	800	mVPP
PLL Response Time (Notes 1 and 2)	$t_{PLL}$	—	—	$t_{out} - 70$	ns

- Notes:
1.  $t_{PLL}$  = the period of time the PLL has from the prescaler rising output transition (50%) to the modulus control input edge transition (50%) to ensure proper modulus selection.
  2.  $t_{out}$  = period of output waveform.

\*2 connected to Pin 3

### PRESCALER BLOCK DIAGRAM



## Product Preview

### ÷128/129 520 MHz LOW-POWER TWO-MODULUS PRESCALER

The MC12018 is a two-modulus prescaler which divides by 128 and 129. An internal regulator is provided to allow this device to be used over a wide range of power-supply voltages. Regulated operation is obtained by connecting supply voltages of 4.5 to 5.5 V to both Pin 7 and Pin 8. Unregulated operation is obtained by connecting voltages greater than 5.5 to Pin 8 and leaving Pin 7 open.

- 520 MHz Toggle Frequency
- Low-Power — 7.0 mA Typical
- Control Input Is Compatible with Standard CMOS and TTL
- Supply Voltage 4.5 V to 9.5 V
- The Specifications of This Product Preview Are Design Goals Only

### MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Regulated Voltage, Pin 7	$V_{reg}$	8.0	Vdc
Power Supply Voltage, Pin 8	$V_{CC}$	10.0	Vdc
Operating Temperature Range	$T_A$	-40 to +85	°C
Storage Temperature Range	$T_{stg}$	-65 to +175	°C

### ELECTRICAL CHARACTERISTICS $(V_{CC} = 5.5 \text{ to } 9.5, V_{reg} = 4.5 \text{ to } 5.5 \text{ V}$ $T_A = -40^\circ\text{C to } +85^\circ\text{C})$

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine Wave Input)	$f_{max}$	520	—	—	MHz
Supply Current (Pin 8)	$I_{CC}$	—	7.0	—	mA
Control Input High ( $\approx 128$ )	$V_{IH}$	2.0	—	—	V
Control Input Low ( $\approx 129$ )	$V_{IL}$	—	—	0.8	V
Differential Output Voltage ( $I_{sink} = 200 \mu\text{A}$ )	$V_{out}$	0.8	1.0	—	V
PLL Response Time (Notes 1 and 2)	$t_{PLL}$	—	—	$t_{out-35}$	ns
Input Voltage Sensitivity	$V_{in}$	200	—	800	mVpp

#### Notes:

1.  $t_{PLL}$  = the period of time the PLL has from the prescaler rising output transition (50%) to the modulus control input edge transition (50%) to ensure proper modulus selection.
2.  $t_{out}$  = period of output waveform

## MC12018

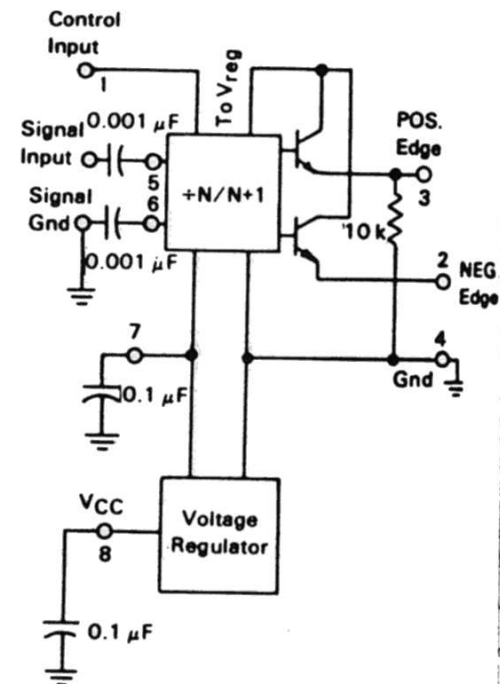
### MECL PLL COMPONENTS

#### ÷128/129 LOW-POWER TWO-MODULUS PRESCALER



P SUFFIX  
PLASTIC PACKAGE  
CASE 626

### PRESCALER BLOCK DIAGRAM



NP 149R1

## Advance Information

### LOW-POWER TWO-MODULUS PRESCALER

The MC12019 is a divide by 20 and 21 two-modulus prescaler. It will divide by 20 when the modulus control input is high and by 21 when the modulus control input is low.

- 225 MHz Toggle Frequency
- Low-Power—7.5 mA Max at 5.5 V
- Control Input Compatible with Standard Motorola CMOS Synthesizers
- Emitter Follower Outputs

### MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Operating Supply Voltage, Pin 7	V <sub>CC</sub>	8.0	Vdc
Operating Temperature Range	T <sub>A</sub>	-40 to +85	°C
Storage Temperature Range	T <sub>stg</sub>	-65 to +175	°C

### ELECTRICAL CHARACTERISTICS (V<sub>CC</sub> = 4.5 to 5.5 V, T<sub>A</sub> = -40° to +85° C)

Characteristic	Symbol	-40°C		25°C		85°C		Unit
		Min	Max	Min	Max	Min	Max	
Toggle Frequency (square wave input)	f <sub>max</sub> f <sub>min</sub>	225	—	225	—	225	—	MHz
Supply Current	I <sub>CC</sub>	—	7.5	—	7.5	—	7.5	mA
Control Input High (20)		2.0	—	2.0	—	2.0	—	V
Control Input Low (20)		—	0.8	—	0.8	—	0.8	V
Output Voltage Swing	V <sub>out</sub>	—	600	—	600	—	600	mV <sub>pp</sub>
Input Voltage Sensitivity	V <sub>in</sub>							
35 MHz		400	800	400	800	400	800	
50-255 MHz		200	800	200	800	200	800	
Response Time (notes 1 and 2)	t <sub>PLL</sub>	—	t <sub>out-70</sub>	—	t <sub>out-70</sub>	—	t <sub>out-70</sub>	ns

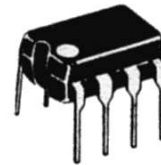
NOTES:

t<sub>PLL</sub> = the time the PLL has from the prescaler rising output transition (50%) to the modulus control input edge transition (50%) to ensure proper modulus selection.

t<sub>out</sub> = period of output waveform.

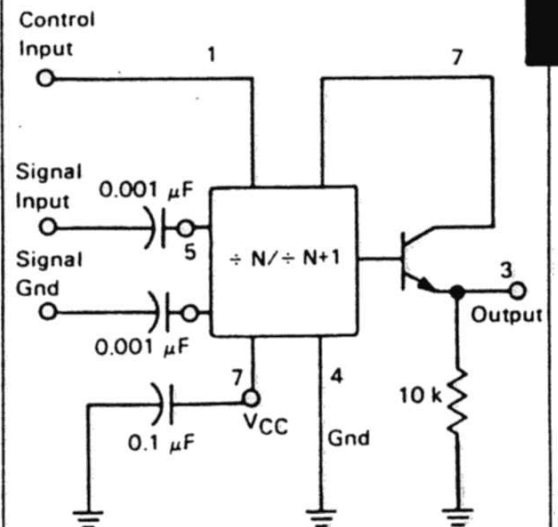
### MECL PLL COMPONENTS

LOW-POWER  
TWO - MODULUS  
PRESCALER  
÷20/21



P SUFFIX  
PLASTIC PACKAGE  
CASE 626

### PRESCALER BLOCK DIAGRAM



5

## Product Preview

### ÷128/129 1.0 GHz LOW-POWER TWO-MODULUS PRESCALER

The MC12022 is a two-modulus prescaler which divides by 128 and 129. An internal regulator is provided to allow this device to be used over a wide range of power-supply voltages. Regulated operation is obtained by connecting supply voltages of 4.5 to 5.5 V to both Pin 7 and Pin 8. Unregulated operation is obtained by connecting voltages greater than 5.5 to Pin 8 and leaving Pin 7 open.

- 1.0 GHz Toggle Frequency
- Low-Power 14 mA Typical
- Control Input Is Compatible with Standard CMOS and TTL
- Supply Voltage 4.5 V to 9.5 V
- Propagation Delay 25 ns Typical
- The Specifications of This Product Preview Are Design Goals Only

### MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Regulated Voltage, Pin 7	$V_{reg}$	8.0	Vdc
Power Supply Voltage, Pin 8	$V_{CC}$	10.0	Vdc
Operating Temperature Range	$T_A$	-40 to +85	°C
Storage Temperature Range	$T_{stg}$	-65 to +175	°C

### ELECTRICAL CHARACTERISTICS ( $V_{CC} = 5.5$ to $9.5$ , $V_{reg} = 4.5$ to $5.5$ V $T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$ )

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine Wave Input)	$f_{max}$	1.0	—	—	GHz
Supply Current (Pin 8)	$I_{CC}$	—	14	—	mA
Control Input High (÷128)	$V_{IH}$	2.0	—	—	V
Control Input Low (÷129)	$V_{IL}$	—	—	0.8	V
Differential Output Voltage ( $I_{sink} = 200 \mu\text{A}$ )	$V_{out}$	0.8	1.0	—	V
PLL Response Time (Notes 1 and 2)	$t_{PLL}$	—	—	$t_{out} - 50$	ns
Input Voltage Sensitivity	$V_{in}$	200	—	800	mVpp

#### Notes:

- $t_{PLL}$  = the period of time the PLL has from the prescaler rising output transition (50%) to the modulus control input edge transition (50%) to ensure proper modulus selection.
- $t_{out}$  = period of output waveform.

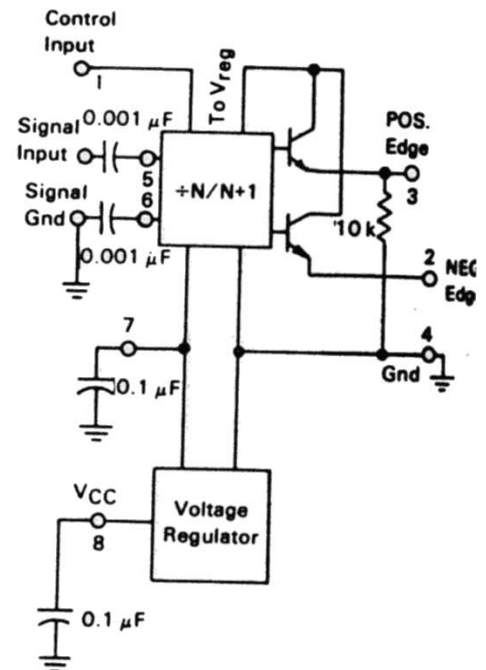
### MECL PLL COMPONENTS

#### ÷128/129 LOW-POWER TWO-MODULUS PRESCALER



P SUFFIX  
PLASTIC PACKAGE  
CASE 626

### PRESCALER BLOCK DIAGRAM



## Advance Information

### ÷ 64, 225 MHz, LOW-POWER PRESCALER

The MC12023 is a new member of Motorola's PLL family. The MC12023 is a prescaler which will divide by 64. This device may be operated over a wide range of supply voltages (3.2 to 5.5 V). Because of this range of supply voltages the MC12023 is very suitable for hand-held, battery-operated devices.

- 225 MHz Toggle Frequency
- Low-Power — 4.0 mA Maximum at 5.5 V
- Operating Supply Voltage — 3.2 V to 5.5 V
- Connecting Pins 2 and 3 Allows Driving One TTL Load

### MINIMUM RATINGS

Characteristic	Symbol	Range	Unit
Supply Voltage	$V_{CC}$	0 to +7.0	Vdc
Operating Temperature Range	$T_A$	0 to +70	°C
Storage Temperature Range	$T_{stg}$	-65 to +175	°C

### TYPICAL CHARACTERISTICS ( $V_{CC} = 3.2$ to $5.5$ V, $T_A = 0^\circ\text{C}$ to $+70^\circ\text{C}$ )

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency (square wave input)	$f_{max}$	225	—	—	MHz
	$f_{min}$	—	—	20	MHz
Current	$I_{CC}$	—	3.5**	4.0	mA
Voltage High* ( $I_{OCE} = 50 \mu\text{A}$ , $V_{CC} = 3.2$ V)	$V_{OH}$	1.2	1.4	—	V
Voltage High* ( $I_{OCE} = 50 \mu\text{A}$ , $V_{CC} = 5.0$ V)	$V_{OH}$	3.5	—	—	V
Voltage Low* ( $I_{OCE} = 2.0$ mA)	$V_{OL}$	—	—	0.5	V
Voltage Sensitivity (15 MHz)	$V_{in}$	400	—	800	mVpp
		200	—	800	
Input Resistance	$R_{in}$	—	TBA	—	k $\Omega$
Input Capacitance	$C_{in}$	—	TBA	—	pF

Connected to Pin 3  
1.5 V

TBA — To Be Announced.

This document contains information on a new product. Specifications and information herein are subject to change without notice.

# MC12023

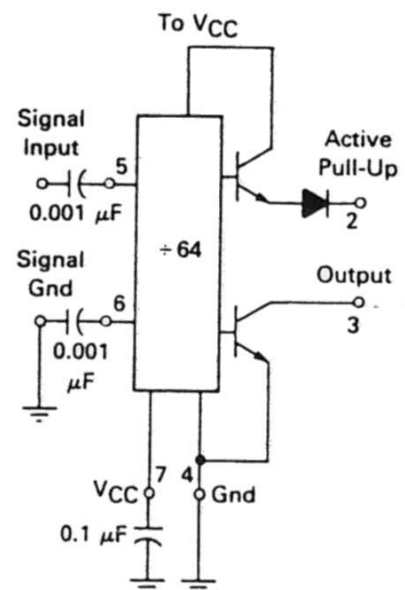
## MECL PLL COMPONENTS

### LOW-POWER PRESCALER ÷ 64



**P SUFFIX**  
PLASTIC PACKAGE  
CASE 626

### PRESCALER BLOCK DIAGRAM





**MOTOROLA**

**MC12040/  
MC12540**

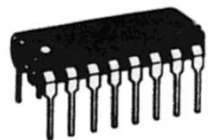
**PHASE-FREQUENCY  
DETECTOR**

The MC12040 is a phase-frequency detector intended for use in systems requiring zero phase and frequency difference at lock. In combination with a voltage controlled oscillator (such as the MC1648), it is useful in a broad range of phase-locked loop applications. Operation of this device is identical to that of Phase Detector #1 of the MC4044. A discussion of the theory of operation and applications information is given on the MC4344/4044 data sheet.

Operating Frequency = 80 MHz typical

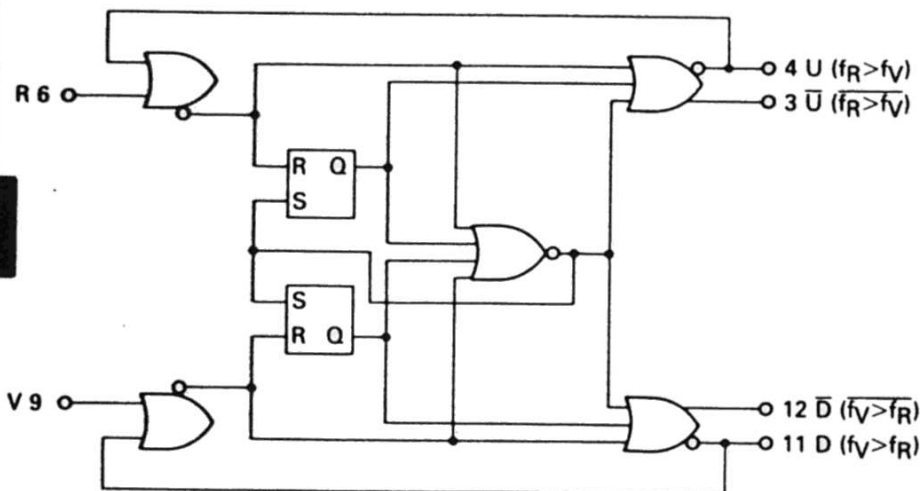
**PHASE-FREQUENCY  
DETECTOR**

**P SUFFIX  
PLASTIC PACKAGE  
CASE 646**



**L SUFFIX  
CERAMIC PACKAGE  
CASE 632-02**

**LOGIC DIAGRAM**



VCC1 = Pin 1  
VCC2 = Pin 14  
VEE = Pin 7

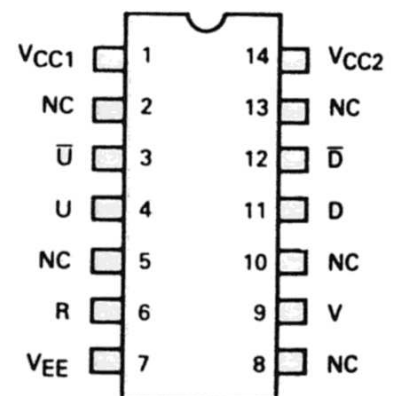
**TRUTH TABLE**

This is not strictly a functional truth table; i.e., it does not cover all possible modes of operation. However it gives a sufficient number of tests to ensure that the device will function properly in all modes of operation.

INPUT		OUTPUT			
R	V	U	D	$\bar{U}$	$\bar{D}$
0	0	X	X	X	X
0	1	X	X	X	X
1	1	X	X	X	X
0	1	X	X	X	X
1	1	1	0	0	1
0	1	1	0	0	1
1	1	1	0	0	1
1	0	1	0	0	1
1	1	0	0	1	1
1	0	0	0	1	1
1	1	0	1	1	0
1	0	0	1	1	0
1	1	0	0	1	0
0	1	0	1	1	0
1	1	0	0	1	0

X = Don't Care

**PIN ASSIGNMENT**



NC — No Connection

5





## CRYSTAL OSCILLATOR

The MC12061 and MC120561 are designed for use with an external crystal to form a crystal controlled oscillator. In addition to the fundamental series mode crystal, two bypass capacitors are required (plus usual power supply pin bypass capacitors). Translators are provided internally for MECL and TTL outputs.

Frequency Range = 2.0 MHz to 20 MHz

Single Supply Operation: + 5.0 Vdc or - 5.2 Vdc

Three Outputs Available:

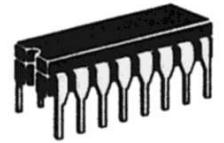
1. Complementary Sine Wave (600 mVp-p typ)
2. Complementary MECL
3. Single Ended TTL

## CRYSTAL OSCILLATOR

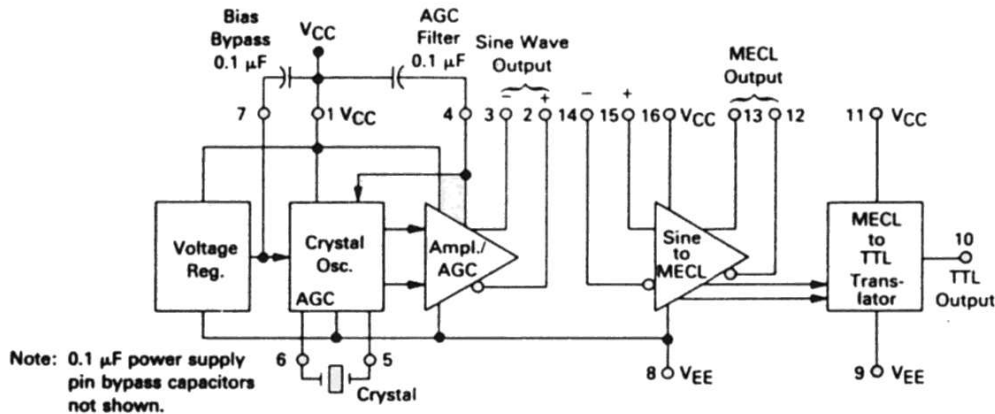
L SUFFIX  
CERAMIC PACKAGE  
CASE 620



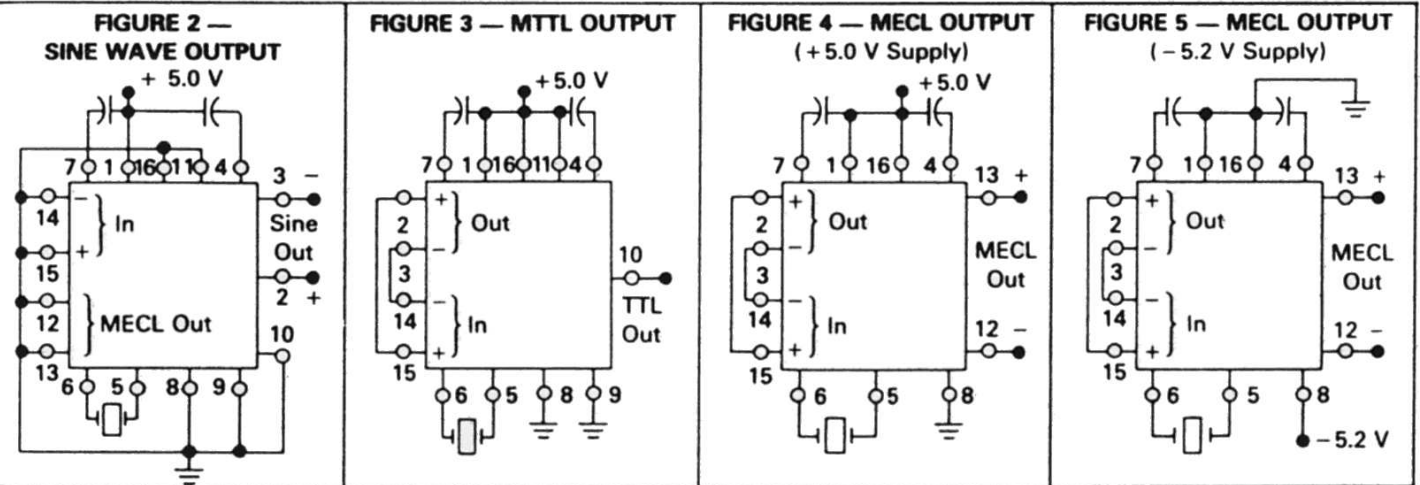
P SUFFIX  
PLASTIC PACKAGE  
CASE 648



## LOGIC DIAGRAM



## TYPICAL CIRCUIT CONFIGURATIONS Note: 0.1 μF power supply pin bypass capacitors not shown.



### CRYSTAL REQUIREMENTS

Note: Start-up stabilization time is a function of crystal series resistance. The lower the resistance, the faster the circuit stabilizes.

Characteristic	MC12061/12561
Mode of Operation	Fundamental Series Resonance
Frequency Range	2.0 MHz - 20 MHz
Series Resistance, R1	Minimum at Fundamental
Maximum Effective Resistance, R <sub>E(max)</sub>	155 ohms

### HIGH-SPEED PRESCALER

The MC12071 is a high-speed prescaler designed for use in communications and instrumentation systems. In the UHF mode, it performs division by 256, and divides by 64 in the VHF mode.

A bandswitch mode control line selects the mode of operation between the UHF and VHF input pins.

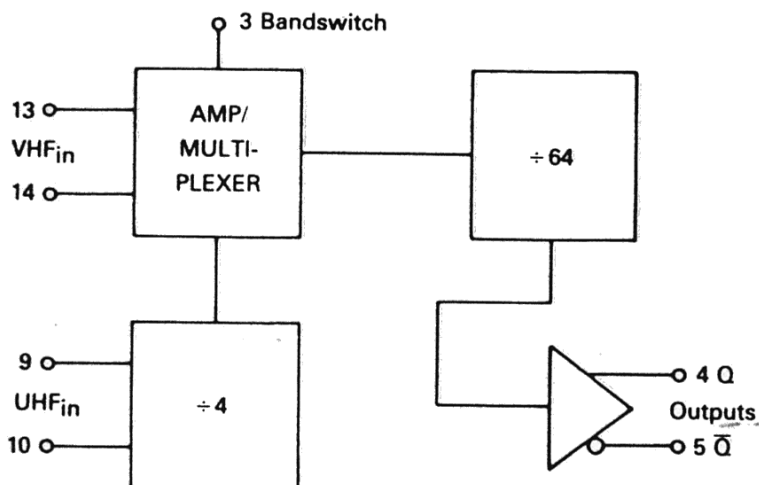
UHF operation is selected by applying a high-level (logical 1) to the bandswitch input. A low-level (logical 0) is applied to the bandswitch input to obtain the VHF mode. An internal amplifier/multiplexer is used to isolate both inputs, amplify the input signal, and improve sensitivity.

Inputs are designed for ac-coupled sine wave signals, but can be dc-coupled if proper bias levels are maintained. Normally used single-ended, the inputs can also be operated with complementary input signals if required.

Circuit outputs are complementary emitter-follower type which can drive a 33-pF or equivalent load. Maintaining a balanced load and controlling rise and fall times will reduce harmonic outputs.

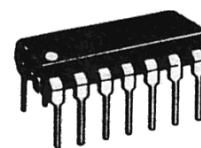
Broadband Operation  
 High Sensitivity  
 Standard 5 Volt Power Supply  
 VHF/UHF — Dual Mode Operation  
 Complementary Emitter-Follower Outputs  
 Independent VHF and UHF Input Pins

### LOGIC DIAGRAM



### HIGH-SPEED PRESCALER

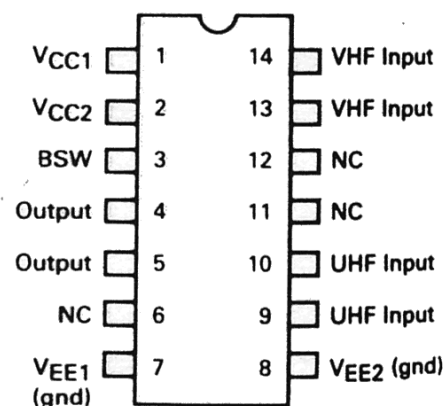
P SUFFIX  
 PLASTIC PACKAGE  
 CASE 646



### TYPICAL APPLICATIONS

- CATV Converters
- Digital frequency synthesizers for:
  - VHF/UHF receivers
  - Instrumentation
  - Satellite communications
- High-frequency divider for:
  - Frequency counters (UHF)
  - Timers (UHF)
  - High-Speed computers
  - SHF, second IF local-oscillator injection
  - Frequency standards
  - PCM communications
  - Radar ranging systems
  - Satellite communications
- High-frequency up-converters

### PIN ASSIGNMENT



NC — No Connection



## Product Preview

### ÷ 64 LOW-POWER PRESCALER

The MC12073 is a new member of Motorola's PLL family. It is a high-speed, low-power prescaler which divides by 64. The MC12073 can be used in all frequency synthesis applications. Typical applications include electronically tuned TV/CATV and communication systems as well as instrumentation.

An internal preamplifier is included in the MC12073. This preamplifier isolates the differential inputs and provides gain for the input signal. The MC12073 is pin compatible with Plessey's SP4632 and has differential outputs.

- 1.1 GHz Toggle Frequency
- Low-Power: 25 mA Typical @  $V_{CC} = 5.0$  V
- High Input Sensitivity
- 800 mV Minimum Peak-Peak Output Swing
- This Product Preview's Specifications are Design Goals Only

### MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Maximum Supply Voltage	$V_{CC}$	7.0	Vdc
Operating Temperature Range	$T_A$	0 to +70	°C
Storage Temperature Range	$T_{stg}$	-65 to +175	°C

### ELECTRICAL CHARACTERISTICS ( $V_{CC} = 4.5$ to $5.5$ V, $T_A = 0^\circ\text{C}$ to $+70^\circ\text{C}$ )

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine wave input)	$f_{max}$	1.1	—	—	GHz
Supply Current	$I_{CC}$	—	25	—	mA
Output Voltage (Load = 10 pF, Sink = 200 $\mu\text{A}$ )	$V_{out}$	0.8	1.0	—	$V_{pp}$
Input Voltage Sensitivity	$V_{in Min}$	—	10	—	mV <sub>rms</sub>
Input Overload	$V_{in Max}$	200	—	—	mV <sub>rms</sub>
Input Resistance	$R_{in}$	—	TBD*	—	k $\Omega$
Input Capacitance	$C_{in}$	—	TBD*	—	pF

\*Not determined.

This document contains information on a new product. Specifications and information herein are subject to change without notice.

## MC12073

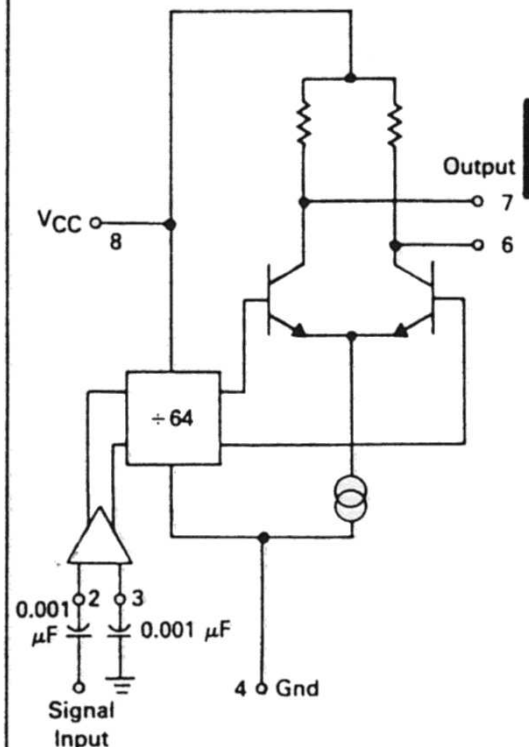
### MECL PLL COMPONENTS

#### LOW-POWER PRESCALER ÷ 64

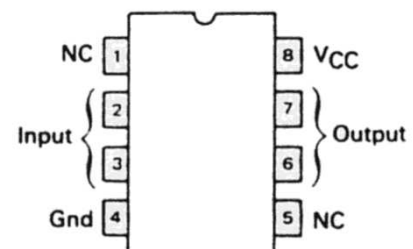


P SUFFIX  
PLASTIC PACKAGE  
CASE 626

### PRESCALER BLOCK DIAGRAM



### PRESCALER PINOUT



5

## Product Preview

### ÷ 256 LOW-POWER PRESCALER

The MC12074 is a new member of Motorola's PLL family. It is a high-speed, low-power prescaler which divides by 256. The MC12074 can be used in all frequency synthesis applications. Typical applications include electronically tuned TV/CATV and communication systems as well as instrumentation.

An internal preamplifier is included in the MC12074. This preamplifier isolates the differential inputs and provides gain for the input signal. The MC12074 is pin compatible with Plessey's SP4653 and has differential outputs.

- 1.1 GHz Toggle Frequency
- Low-Power: 25 mA Typical @  $V_{CC} = 5.0\text{ V}$
- High Input Sensitivity
- 800 mV Minimum Peak-Peak Output Swing
- This Product Preview's Specifications are Design Goals Only

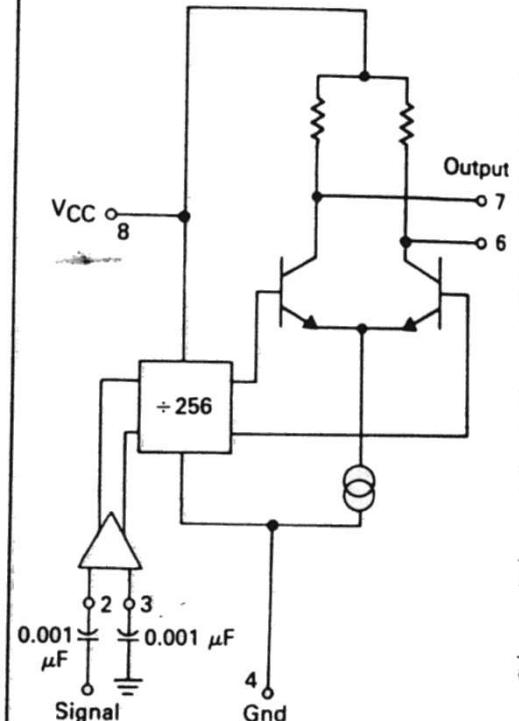
### MECL PLL COMPONENTS

#### LOW-POWER PRESCALER ÷ 256

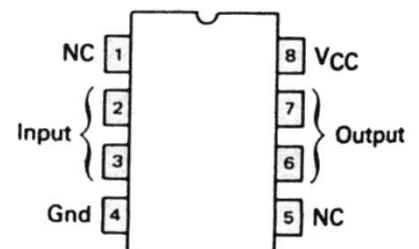


**P SUFFIX  
PLASTIC PACKAGE  
CASE 626**

### PRESCALER BLOCK DIAGRAM



### PRESCALER PINOUT



5

### MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Power Supply Voltage	$V_{CC}$	7.0	Vdc
Operating Temperature Range	$T_A$	0 to +70	°C
Storage Temperature Range	$T_{stg}$	-65 to +175	°C

### ELECTRICAL CHARACTERISTICS ( $V_{CC} = 4.5$ to $5.5\text{ V}$ , $T_A = 0^\circ\text{C}$ to $+70^\circ\text{C}$ )

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine wave input)	$f_{max}$	1.1	—	—	GHz
Supply Current	$I_{CC}$	—	25	—	mA
Output Voltage (Load = 10 pF, $I_{sink} = 200\ \mu\text{A}$ )	$V_{out}$	0.8	1.0	—	$V_{pp}$
Input Voltage Sensitivity	$V_{in\ Min}$	—	10	—	mV <sub>rms</sub>
Input Overload	$V_{in\ Max}$	200	—	—	mV <sub>rms</sub>
AC Input Resistance	$R_{in}$	—	TBD*	—	k $\Omega$
Input Capacitance	$C_{in}$	—	TBD*	—	pF

\*To be determined.

This document contains information on a new product. Specifications and information herein are subject to change without notice.

## Advance Information

### UHF PRESCALER

The MC12090 is a high-speed D master-slave flip-flop capable of toggle rates of over 700 MHz. It was designed primarily for high-speed prescaling applications in communications and instrumentation. This device employs two data inputs, two clock inputs as well as complementary Q and  $\bar{Q}$  outputs. There are no SET or RESET inputs.

### PLL COMPONENTS

#### HIGH-SPEED PRESCALER

### ELECTRICAL CHARACTERISTICS

Characteristic	Symbol	0°		25°		75°		Unit
		Min	Max	Min	Max	Min	Max	
Power Supply Current	$I_E$	—	65	—	59	—	65	mA
Output Current High (Pin 7, 9)	$I_{inH}$	—	400	—	260	—	260	$\mu A$
Output Current High (Pin 11, 12)	$I_{inH}$	—	435	—	280	—	280	$\mu A$
Output Current Low	$I_{inL}$	0.5	—	0.5	—	0.3	—	$\mu A$
High Output Voltage	$V_{OH}$	-1.02	-0.84	-0.98	-0.81	-0.92	-0.735	Vdc
Low Output Voltage	$V_{OL}$	-1.95	-1.63	-1.95	-1.63	-1.95	-1.60	Vdc
High Input Voltage	$V_{IH}$	-1.17	-0.84	-1.13	-0.81	-1.70	-0.735	Vdc
Low Input Voltage	$V_{IL}$	-1.87	-1.495	-1.85	-1.48	-1.83	-1.45	Vdc

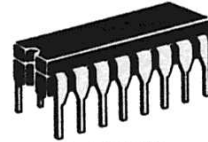
### PARAMETERS

Characteristic	Symbol	0°C		25°C		75°C		Unit
		Min	Max	Min	Max	Min	Max	
Toggle Frequency	$f_{tog}$	700	—	750	—	700	—	MHz

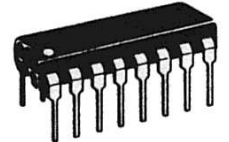
#### Typical (25°C)

Propagation Delay Clock to Output (Pins 7 & 9-2)	$t_{pd}$	1.3						ns
Setup Time setup H setup L	$t_s$			0.3				ns
Hold Time hold H hold L	$t_h$			0.2				ns
Rise Time	$t_r$			0.9				ns
Fall Time	$t_f$			0.9				ns

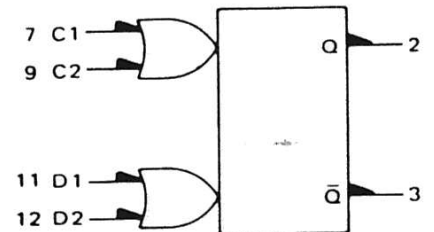
### P SUFFIX PLASTIC PACKAGE CASE 648



L SUFFIX  
CERAMIC PACKAGE  
CASE 620



### LOGIC DIAGRAM



$V_{CC1}$  = Pin 1  
 $V_{CC2}$  = Pin 16  
 $V_{EE}$  = Pin 8

### TRUTH TABLE

C	D	$Q_{n+1}$
L	$\phi$	$Q_n$
H	$\phi$	$Q_n$
	L	L
	H	H

C = C1 + C2       $\phi$  = Don't Care  
D = D1 + D2

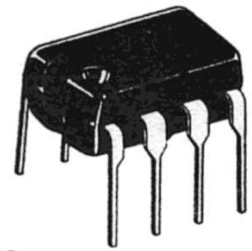
**Advance Information**
**FM MODULATOR CIRCUIT**

... a voltage-controlled oscillator/modulator ideally suited to cordless telephone and television intercarrier applications.

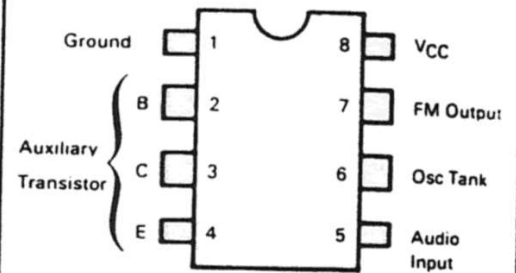
- Wide Supply Range (5.0-12 Vdc)
- Useful Frequency Range (1.4-14 MHz)
- Low Distortion (<1%)
- Excellent Oscillator Stability
- Output RF Driver Transistor Included
- Low Cost, Low Component Count Circuit
- Wide Deviation Capability

**FM MODULATOR CIRCUIT**

SILICON MONOLITHIC  
INTEGRATED CIRCUIT

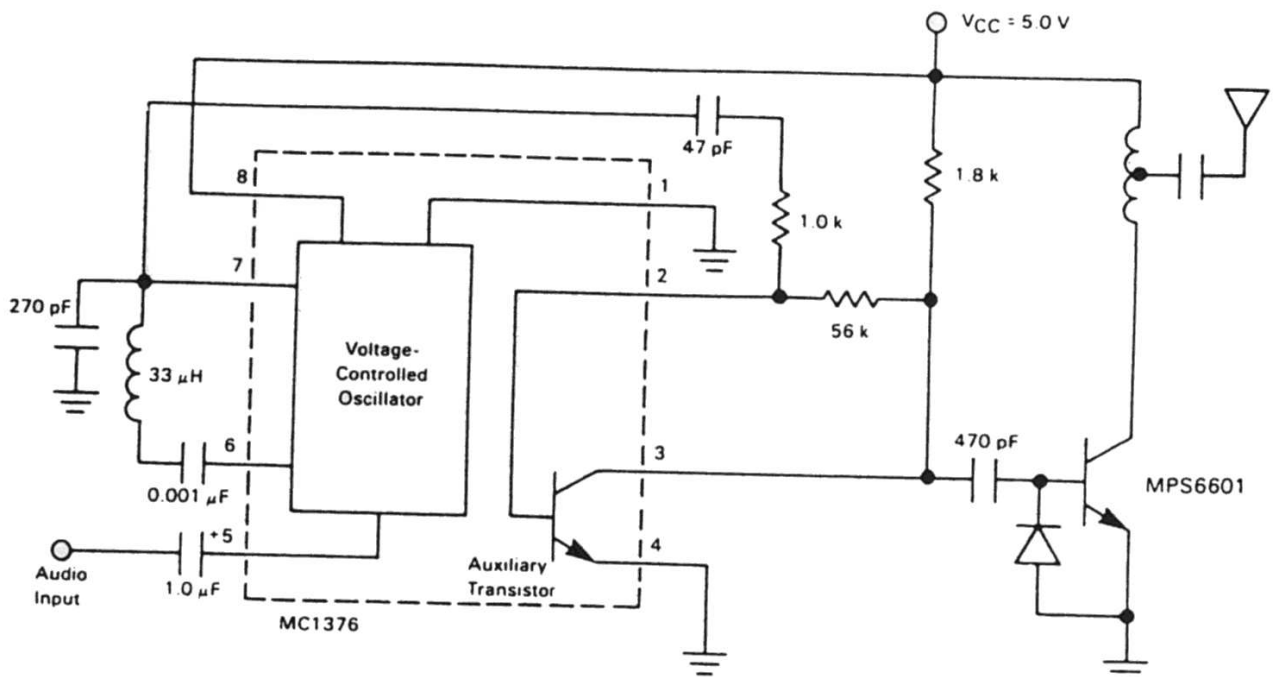


CASE 626



5

FIGURE 1 — CORDLESS TELEPHONE BASE STATION TRANSMITTER (1.76 MHz)





**MOTOROLA**

**MC14046B**

**PHASE-LOCKED LOOP**

The MC14046B phase-locked loop contains two phase comparators, a voltage-controlled oscillator (VCO), source follower, and zener diode. The comparators have two common signal inputs.  $PCA_{in}$  and  $PCB_{in}$ . Input  $PCA_{in}$  can be used directly coupled to large voltage signals, or indirectly coupled (with a series capacitor) to small voltage signals. The self-bias circuit adjusts small voltage signals in the linear region of the amplifier. Phase comparator 1 (an exclusive OR gate) provides a digital error signal  $PC1_{out}$ , and maintains  $90^\circ$  phase shift at the center frequency between  $PCA_{in}$  and  $PCB_{in}$  signals (both at 50% duty cycle). Phase comparator 2 (with leading edge sensing logic) provides digital error signals  $PC2_{out}$  and  $PCP_{out}$ , and maintains a  $0^\circ$  phase shift between  $PCA_{in}$  and  $PCB_{in}$  signals (duty cycle is immaterial). The linear VCO produces an output signal  $VCO_{out}$  whose frequency is determined by the voltage of input  $VCO_{in}$  and the capacitor and resistors connected to pins  $C1A$ ,  $C1B$ ,  $R1$ , and  $R2$ . The source-follower output  $SF_{out}$  with an external resistor is used where the  $VCO_{in}$  signal is needed but no loading can be tolerated. The inhibit input  $Inh$ , when high, disables the VCO and source follower to minimize standby power consumption. The zener diode can be used to assist in power supply regulation.

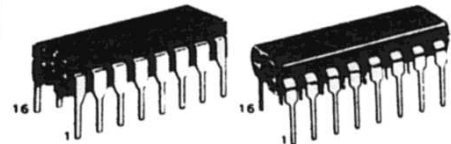
Applications include FM and FSK modulation and demodulation, frequency synthesis and multiplication, frequency discrimination, tone decoding, data synchronization and conditioning, voltage-to-frequency conversion and motor speed control.

- VCO Frequency = 1.4 MHz Typical @  $V_{DD} = 10$  Vdc
- VCO Frequency Drift with Temperature = 0.04%/°C Typical @  $V_{DD} = 10$  Vdc
- VCO Linearity = 1% Typical
- Quiescent Current = 5.0 nA/package typical @ 5 Vdc
- Low Dynamic Power Dissipation – 70  $\mu$ W Typical @  $f_0 = 10$  kHz,  $V_{DD} = 5.0$  Vdc,  $R1 = 1.0$  M $\Omega$ ,  $R2 = \infty$ ,  $R_{SF} = \infty$
- Buffered Outputs Compatible with MHTL and Low-Power TTL
- Diode Protection on All Inputs
- Supply Voltage Range = 3.0 to 18 Vdc
- Pin-for-Pin Replacement for CD4046B
- Phase Comparator 1 is an Exclusive Or Gate and is Duty Cycle Limited
- Phase Comparator 2 switches on Rising Edges and is not Duty Cycle Limited

**CMOS MSI**

(LOW-POWER COMPLEMENTARY MOS)

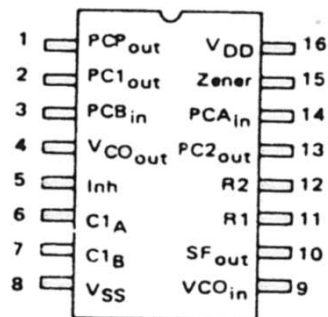
**PHASE-LOCKED LOOP**



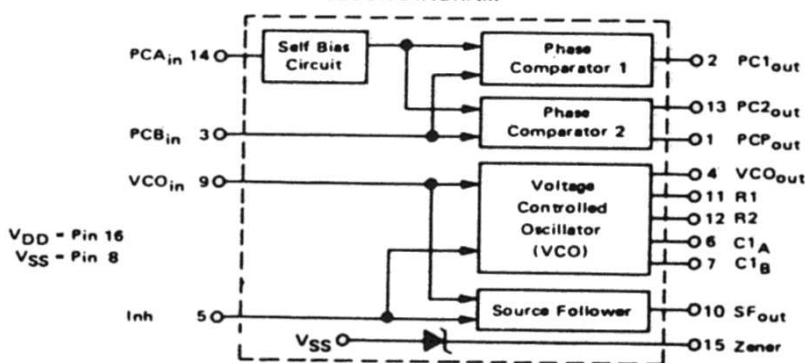
**L SUFFIX**  
CERAMIC PACKAGE  
CASE 620

**P SUFFIX**  
PLASTIC PACKAGE  
CASE 648

**PIN ASSIGNMENT**



**BLOCK DIAGRAM**



This device contains circuitry to protect the inputs against damage due to high static voltages or electric fields; however, it is advised that normal precautions be taken to avoid application of any voltage higher than maximum rated voltages to this high impedance circuit. For proper operation it is recommended that  $V_{in}$  and  $V_{out}$  be constrained to the range  $V_{SS} < (V_{in} \text{ or } V_{out}) < V_{DD}$ .

Unused inputs must always be tied to an appropriate logic voltage level (e.g., either  $V_{SS}$  or  $V_{DD}$ ). Pins 6, 7, 10, 11, 12, and 15 if unused must be left open.

**5**



**MOTOROLA**

**MC145106**

**PLL FREQUENCY SYNTHESIZER**

The MC145106 is a phase locked loop (PLL) frequency synthesizer constructed in CMOS on a single monolithic structure. This synthesizer finds applications in such areas as CB and FM transceivers. The device contains an oscillator/amplifier, a  $2^{10}$  or  $2^{11}$  divider chain for the oscillator signal, a programmable divider chain for the input signal and a phase detector. The MC145106 has circuitry for a 10.24 MHz oscillator or may operate with an external signal. The circuit provides a 5.12 MHz output signal, which can be used for frequency tripling. A  $2^9$  programmable divider divides the input signal frequency for channel selection. The inputs to the programmable divider are standard ground-to-supply binary signals. Pull-down resistors on these inputs normally set these inputs to ground enabling these programmable inputs to be controlled from a mechanical switch or electronic circuitry.

The phase detector may control a VCO and yields a high level signal when input frequency is low, and a low level signal when input frequency is high. An out of lock signal is provided from the on-chip lock detector with a "0" level for the out of lock condition.

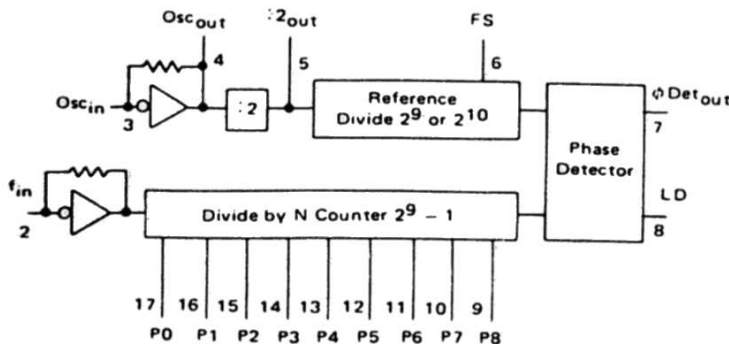
- Single Power Supply
- Wide Supply Range: 4.5 to 12 V
- Provision for 10.24 MHz Crystal Oscillator
- 5.12 MHz Output
- Programmable Division Binary Input Selects up to  $2^9$
- On-Chip Pull Down Resistors on Programmable Divider Inputs
- Selectable Reference Divider,  $2^{10}$  or  $2^{11}$  (including + 2)
- Three-State Phase Detector
- Pin-for-Pin Replacement for MM55106, MM55116
- Chip Complexity: 880 FETs or 220 Equivalent Gates

**CMOS MSI**  
(LOW-POWER COMPLEMENTARY MOS)  
**PLL**  
**FREQUENCY SYNTHESIZER**



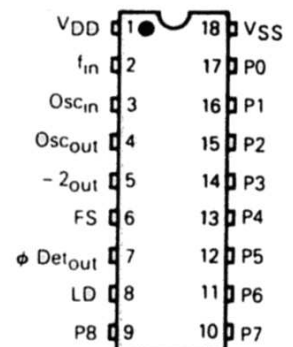
**P SUFFIX**  
PLASTIC PACKAGE  
CASE 707

**BLOCK DIAGRAM**



VDD Pin 1  
VSS Pin 18

**PIN ASSIGNMENT**



5



# MC145145

## Advance Information

### 4-BIT DATA BUS INPUT PLL FREQUENCY SYNTHESIZER

The MC145145 is one of a family of LSI PLL frequency synthesizer parts from Motorola CMOS. The family includes devices having serial, parallel and 4-bit data bus programmable inputs. Options include single- or dual-modulus capability, transmit/receive offsets, choice of phase detector types and choice of reference divider integer values.

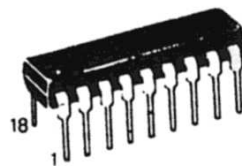
The MC145145 is programmed by a 4-bit input, with strobe and address lines. The device features consist of a reference oscillator, 12-bit programmable reference divider, digital-phase detector, 14-bit programmable divide-by-N counter and the necessary latch circuitry for accepting the 4-bit input data. When combined with a loop filter and VCO, the MC145145 can provide all the remaining functions for a PLL frequency synthesizer operating up to the device's frequency limit. For higher VCO frequency operation, a down mixer or a fixed divide prescaler can be used between the VCO and MC145145.

- General Purpose Applications
  - CATV
  - TV Tuning
  - AM/FM Radios
  - Scanning Receivers
  - Two Way Radios
  - Amateur Radio
- Low Power Drain
- 3.0 to 9.0 Vdc Supply Range
- >30 MHz Typical Input Capability @5 Vdc
- Programmable Reference Divider for Values Between 3 and 4095
- On- or Off-Chip Reference Oscillator Operation
- Single Modulus 4-Bit Data Bus Programming
- +N Range = 3 to 16383
- "Linearized" Digital Phase Detector Enhances Transfer Function Linearity
- Two Error Signal Options –
  - Single Ended (Three State)
  - Double Ended

### CMOS LSI

(LOW-POWER COMPLEMENTARY MOS)

### 4-BIT DATA BUS INPUT PLL FREQUENCY SYNTHESIZER

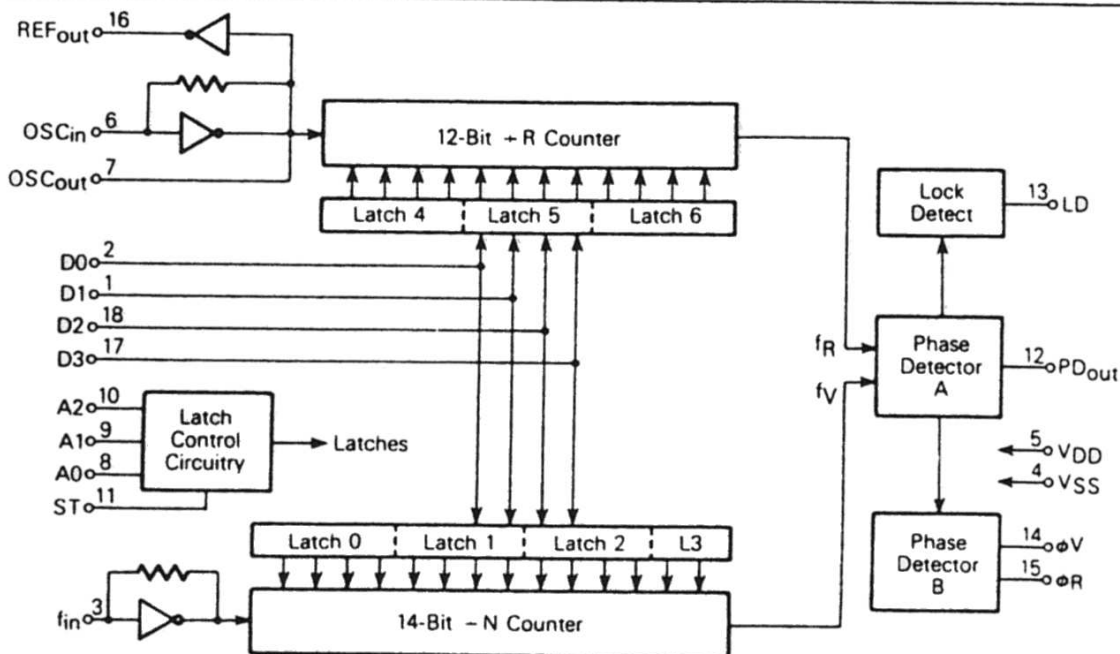


P SUFFIX  
PLASTIC PACKAGE  
CASE 707

#### PIN ASSIGNMENT

D1	1	18	D2
D0	2	17	D3
f <sub>in</sub>	3	16	REF <sub>out</sub>
VSS	4	15	φ <sub>R</sub>
VDD	5	14	φ <sub>V</sub>
OSC <sub>in</sub>	6	13	LD
OSC <sub>out</sub>	7	12	PD <sub>out</sub>
A0	8	11	ST
A1	9	10	A2

5







**PARALLEL INPUT PLL FREQUENCY SYNTHESIZER**

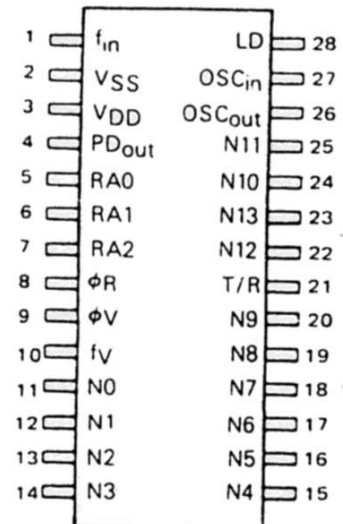
The MC145151 is one of a family of LSI PLL frequency synthesizer parts from Motorola CMOS. The family includes devices having serial, parallel and 4-bit data bus programmable inputs. Options include single- or dual-modulus capability, transmit/receive offsets, choice of phase detector types and choice of reference divider integer values.

The MC145151 is programmed by 14 parallel input-data lines. The device features consist of a reference oscillator, selectable-reference divider, digital-phase detector and 14-bit programmable divide-by-N counter. When combined with a loop filter and VCO, the MC145151 can provide all the remaining functions for a PLL frequency synthesizer operating up to the device's frequency limit. For higher VCO frequency operation, a down mixer or a fixed divide prescaler can be used between the VCO and MC145151.

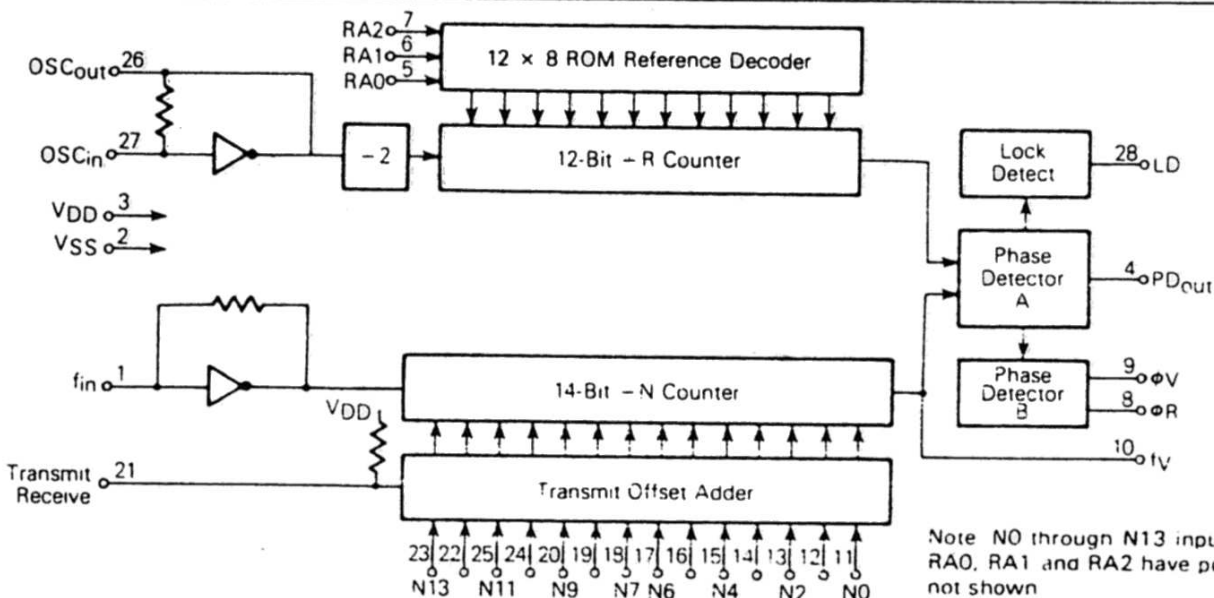
- General Purpose Applications –
  - CATV
  - AM/FM Radios
  - Two-Way Radios
  - TV Tuning
  - Scanning Receivers
  - Amateur Radio
- Low Power Drain
- 3.0 to 9.0 Vdc Supply Range
- >30 MHz Typical Input Capability @ 5 Vdc
- 8 User Selectable Reference Divider Values – 8, 128, 256, 512, 1024, 2048, 2410, 8192
- On- or Off-Chip Reference Oscillator Operation
- Lock Detect Signal
- +N Counter Output Available
- Single Modulus/Parallel Programming
- +N Range = 3 to 16383
- "Linearized" Digital Phase Detector Enhances Transfer Function Linearity
- Two Error Signal Options –
  - Single Ended (Three-State)
  - Double Ended



**P SUFFIX**  
PLASTIC PACKAGE  
CASE 710



5



Note N0 through N13 inputs and inputs RA0, RA1 and RA2 have pullup resistors not shown



## PARALLEL INPUT PLL FREQUENCY SYNTHESIZER

The MC145152 is one of a family of LSI PLL frequency synthesizer parts from Motorola CMOS. The family includes devices having serial, parallel and 4-bit data bus programmable inputs. Options include single- or dual-modulus capability, transmit/receive offsets, choice of phase detector types and choice of reference divider integer values.

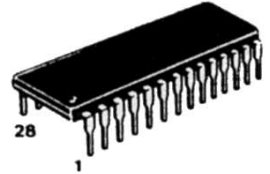
The MC145152 is programmed by sixteen parallel inputs. The device features consist of a reference oscillator, selectable-reference divider, two output phase detector, 10-bit programmable divide-by-N counter and 6-bit programmable +A counter. When combined with a loop filter and VCO, the MC145152 can provide all the remaining functions for a PLL frequency synthesizer operating up to the device's frequency limit. For higher VCO frequency operation, a down mixer or a dual modulus prescaler can be used between the VCO and MC145152.

- General Purpose Applications –
  - CATV                      TV Tuning
  - AM/FM Radios          Scanning Receivers
  - Two-Way Radios        Amateur Radio
- Low Power Drain
- 3.0 to 9.0 Vdc Supply Range
- >30 MHz Typical Input Capability @ 5 Vdc
- 8 User Selectable Reference Divider Values – 8, 64, 128, 256, 512, 1024, 1160, 2048
- On- or Off-Chip Reference Oscillator Operation
- Lock Detect Signal
- Dual Modulus/Parallel Programming
- +N Range = 3 to 1023
- +A Range = 0 to 63

## CMOS LSI

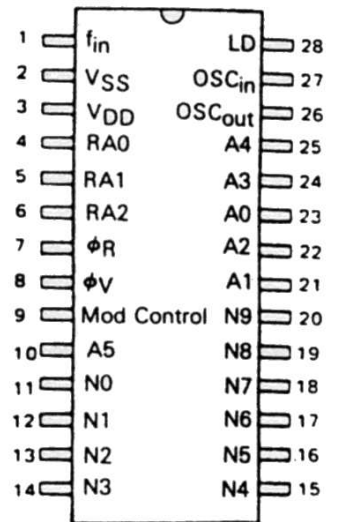
(LOW POWER COMPLEMENTARY MOS)

## PARALLEL INPUT PLL FREQUENCY SYNTHESIZER

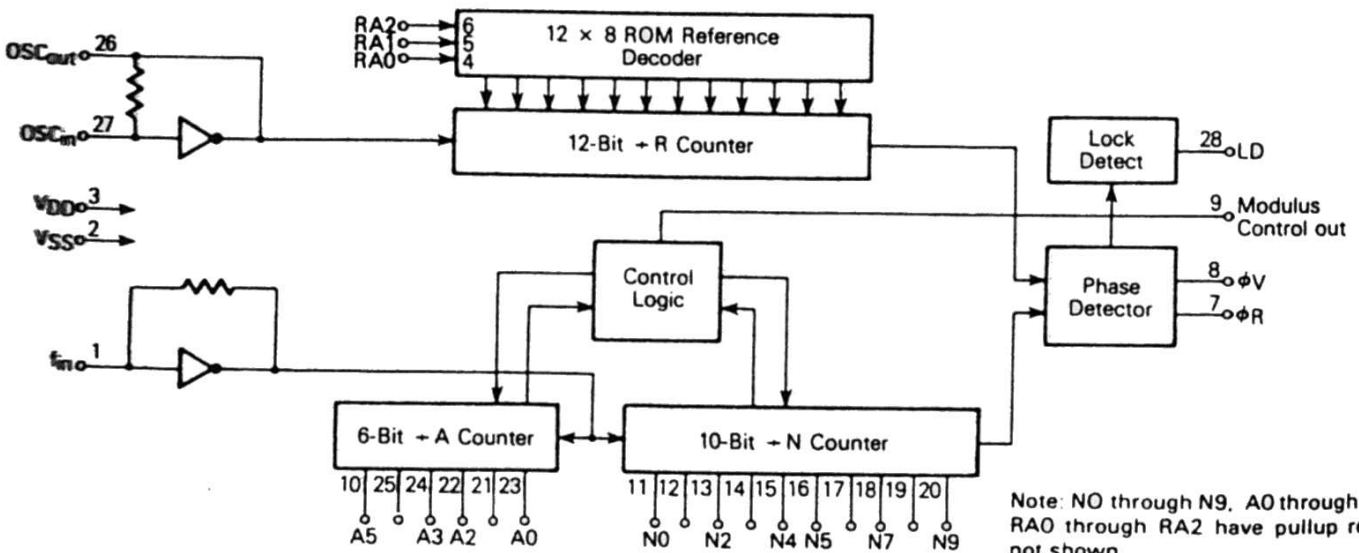


**P SUFFIX**  
PLASTIC PACKAGE  
CASE 710-02

### PIN ASSIGNMENT



5



# MC145155

## CMOS LSI

(LOW-POWER COMPLEMENTARY MOS)

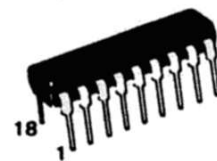
## SERIAL INPUT PLL FREQUENCY SYNTHESIZER

### SERIAL INPUT PLL FREQUENCY SYNTHESIZER

The MC145155 is one of a family of LSI PLL Frequency synthesizer parts from Motorola CMOS. The family includes devices having serial, parallel and 4-bit data bus programmable inputs. Options include single- or dual-modulus capability, transmit/receive offsets, choice of phase detector types and choice of reference divider integer values.

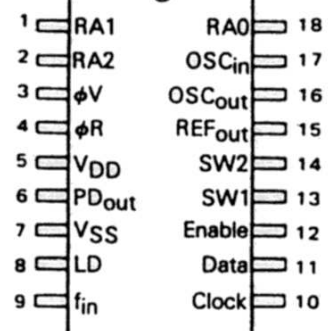
The MC145155 is programmed by a clocked, serial input, 16-bit data stream. The device features consist of a reference oscillator, selectable-reference divider, digital-phase detector, 14-bit programmable divide-by-N counter and the necessary shift register and latch circuitry for accepting the serial input data. When combined with a loop filter and VCO, the MC145155 can provide all the remaining functions for a PLL frequency synthesizer operating up to the device's frequency limit. For higher VCO frequency operation, a down mixer or a fixed divide prescaler can be used between the VCO and MC145155.

- General Purpose Applications –
  - CATV                      TV Tuning
  - AM/FM Radios        Scanning Receivers
  - Two-Way Radios    Amateur Radio
- Low Power Drain
- 3.0 to 9.0 Vdc Supply Range
- >30 MHz Typical Input Capability @ 5 Vdc
- 8 User Selectable Reference Divider Values – 16, 512, 1024, 2048, 3668, 4096, 6144, 8192
- On- or Off-Chip Reference Oscillator Operation with Buffered Output
- Lock Detect Signal
- Two Open-Drain Switch Outputs
- Single Modulus/Serial Programming
- + N Range = 3 to 16383
- "Linearized" Digital Phase Detector Enhances Transfer Function Linearity
- Two Error Signal Options –
  - Single Ended (Three-State)
  - Double Ended

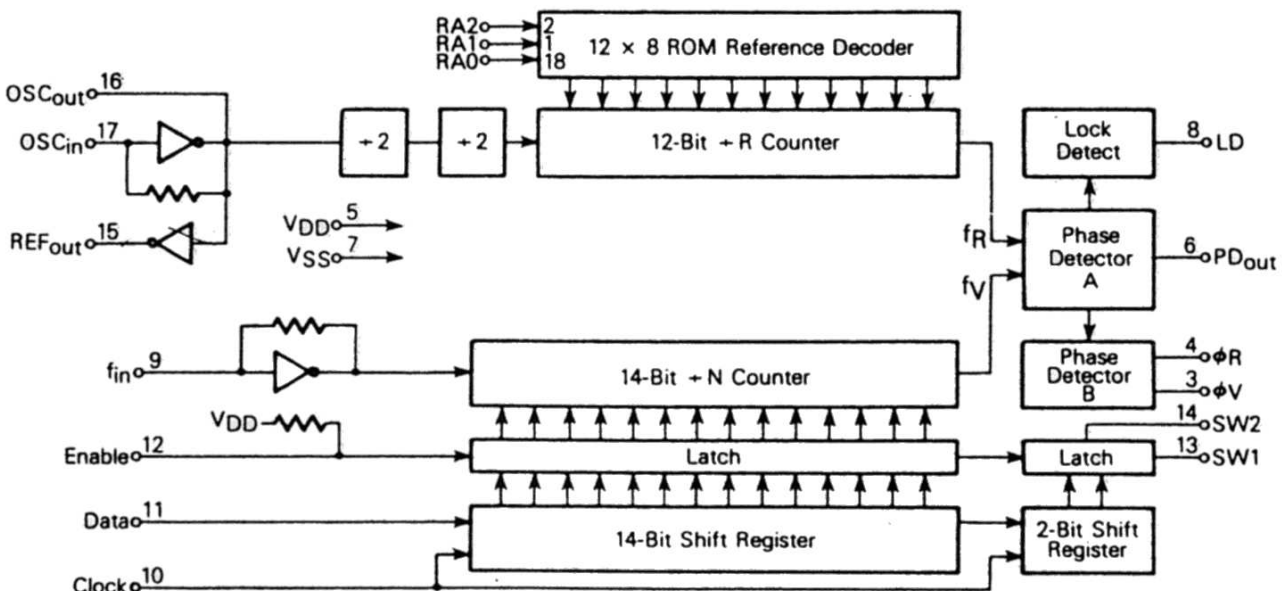


P SUFFIX  
PLASTIC PACKAGE  
CASE 707

### PIN ASSIGNMENT



5



**SERIAL INPUT PLL FREQUENCY SYNTHESIZER**

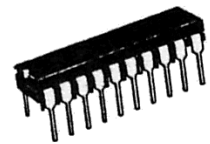
The MC145156 is one of a family of LSI PLL frequency synthesizer parts from Motorola CMOS. The family includes devices having serial, parallel and 4-bit data bus programmable inputs. Options include single- or dual-modulus capability, transmit/receive offsets, choice of phase detector types and choice of reference divider integer values.

The MC145156 is programmed by a clocked, serial input, 19-bit data stream. The device features consist of a reference oscillator, selectable-reference divider, digital-phase detector, 10-bit programmable divide-by-N counter, 7-bit programmable +A counter and the necessary shift register and latch circuitry for accepting the serial input data. When combined with a loop filter and VCO, the MC145156 can provide all the remaining functions for a PLL frequency synthesizer operating up to the device's frequency limit. For higher VCO frequency operation, a down mixer or a dual modulus prescaler can be used between the VCO and MC145156.

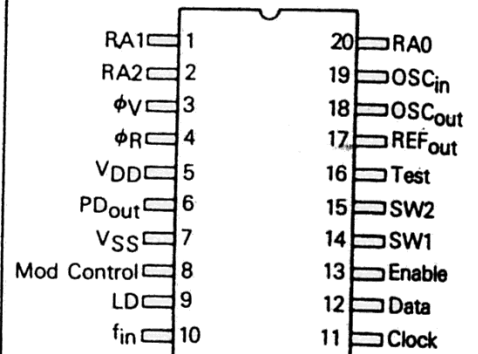
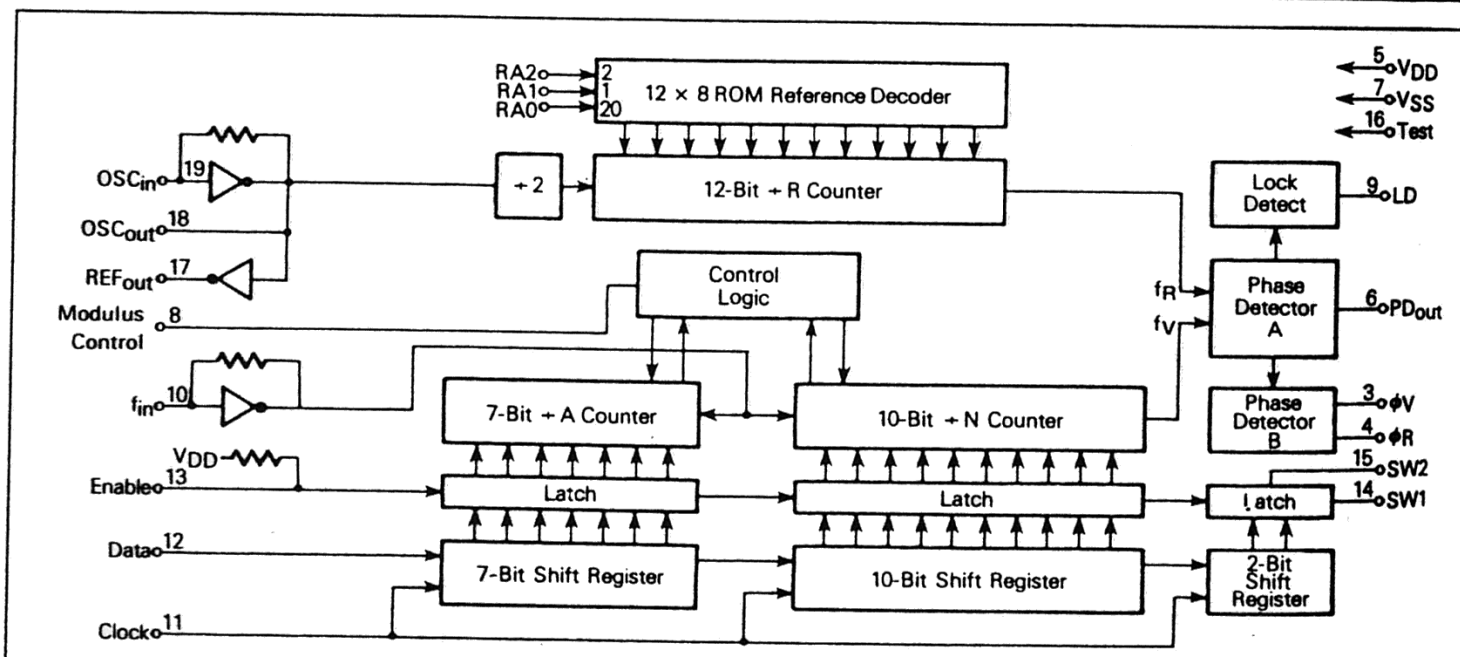
- General Purpose Applications —
  - CATV                      TV Tuning
  - AM/FM Radios        Scanning Receivers
  - Two-Way Radios     Amateur Radio
- Low Power Drain
- 3.0 to 9.0 Vdc Supply Range
- >30 MHz Typical Input Capability @ 5 Vdc
- 8 User Selectable Reference Divider Values — 8, 64, 128, 256, 640, 1000, 1024, 2048
- On- or Off-Chip Reference Oscillator Operation with Buffered Output
- Lock Detect Signal
- Two Open-Drain Switch Outputs
- Dual Modulus/Serial Programming
- +N Range = 3 to 1023
- "Linearized" Digital Phase Detector Enhances Transfer Function Linearity
- Two Error Signal Options —
  - Single Ended (Three-State)
  - Double Ended

**CMOS LSI**

(LOW-POWER COMPLEMENTARY MOS)

**SERIAL INPUT PLL  
FREQUENCY SYNTHESIZER**


**P SUFFIX**  
PLASTIC PACKAGE  
CASE 738-02

**PIN ASSIGNMENT**

**5**






# MC145159-1

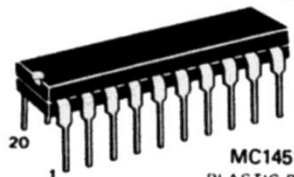
## Advance Information

### SERIAL INPUT PLL FREQUENCY SYNTHESIZER WITH ANALOG PHASE DETECTOR

The MC145159-1 has a programmable 14-bit reference counter, as well as programmable divide-by-N/divide-by-A counters. The counters are programmed serially through a common data input and latched into the appropriate counter latch, according to the last data bit (control bit) entered.

When combined with a loop filter and VCO, this device can provide all the remaining functions for a PLL frequency synthesizer operating up to the device's frequency limit. For higher VCO frequency operations, a down mixer or a dual modulus prescaler can be used between the VCO and the PLL.

- General Purpose Applications:
  - CATV TV Tuning
  - AM/FM Radios Scanning Receivers
  - Two Way Radios Amateur Radio
- Low Power Consumption
- 3.0 to 9.0 V Supply Range
- On- or Off-Chip Reference Oscillator Operation
- Dual Modulus
- Compatible with the Serial Peripheral Interface (SPI) on CMOS MCUs
- $\div R$  Range = 3 to 16383
- $\div N$  Range = 16 to 1023,  $\div A$  Range = 0 to 127
- High-Gain Analog Phase Detector

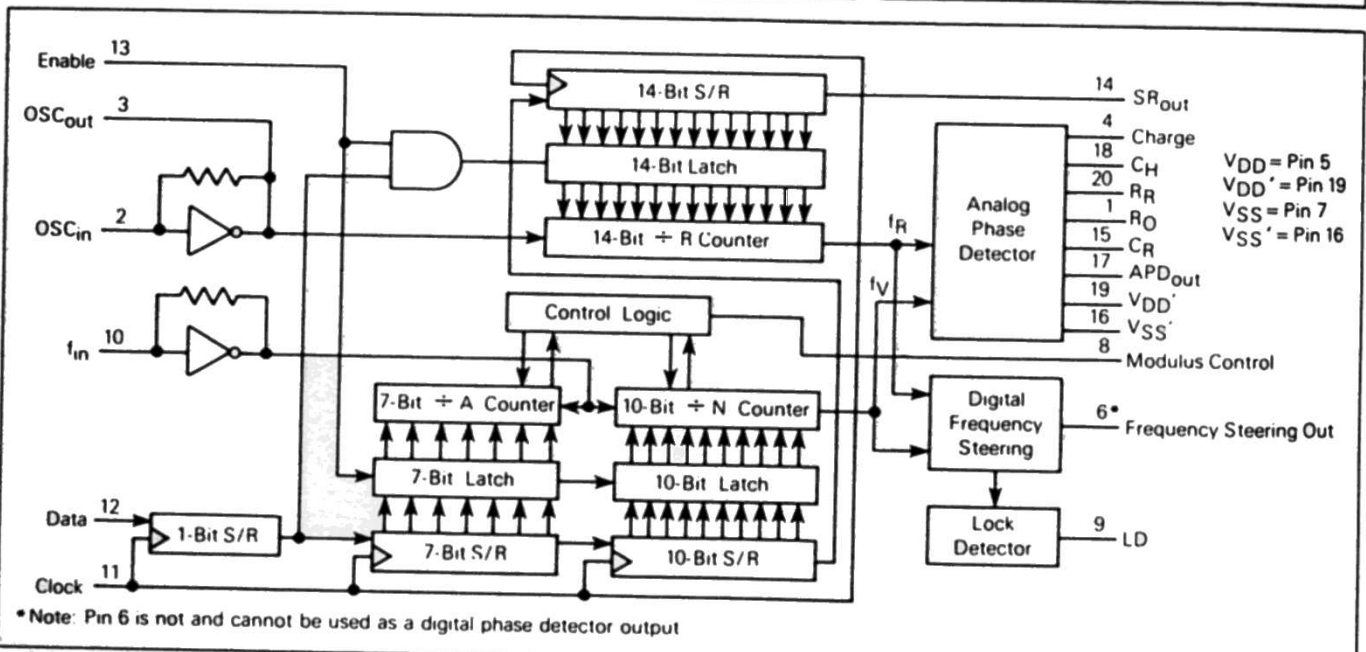


MC145159P1  
PLASTIC PACKAGE  
CASE 738

### PIN ASSIGNMENT

RO	1	20	RR
OSC <sub>in</sub>	2	19	VDD'
OSC <sub>out</sub>	3	18	CH
Charge	4	17	APD <sub>out</sub>
VDD	5	16	VSS'
Frequency Steering Out	6	15	CR
VSS	7	14	SR <sub>out</sub>
Modulus Control	8	13	Enable
LD	9	12	Data
f <sub>in</sub>	10	11	Clock

5



\* Note: Pin 6 is not and cannot be used as a digital phase detector output

This document contains information on a new product. Specifications and information herein are subject to change without notice.





**MOTOROLA**

**MC145160  
MC145161**

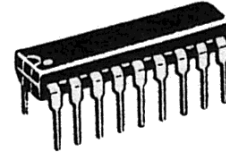
**Product Preview**

**DUAL PLL**

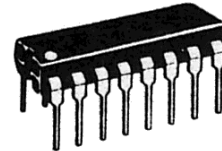
The MC145160 is a dual phase locked loop frequency synthesizer intended for use primarily in 46/49 MHz cordless phone. The part contains two ROM programmable counters for receive and transmit loops with two independent phase detect circuits. A common reference oscillator and reference divider is shared by the receive and transmit circuits.

Other features include a lock detect circuit for the transmit loop, illegal code default, a buffered oscillator output for mixing purposes in the system, 5 KHz and 4 KHz tone output. The reference oscillator can also be optioned to accept an 11.15 MHz crystal.

- FCC 46/49 MHz Cordless Phone Channel ROM
- On-chip PLL for transmit/receive
- On-chip Oscillator with Buffered Output
- Low Power Consumption
- 3.0 to 5.5V Supply Range
- Lock Detect Signal
- 5 KHz/4 KHz Output

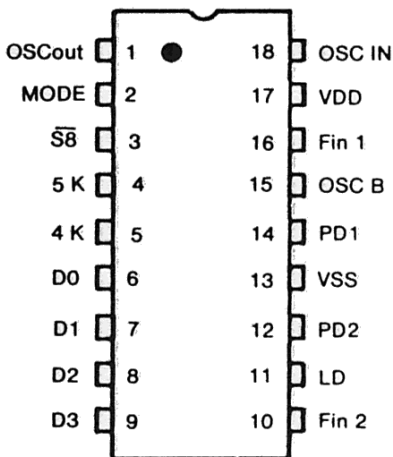


CASE 707-02  
PLASTIC

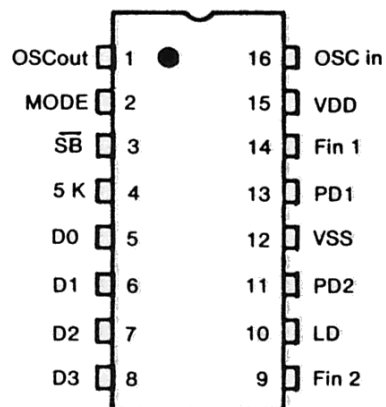


CASE 648  
PLASTIC

**PIN ASSIGNMENT**



MC145160



MC145161

**5**



**MOTOROLA**

**MC145163**

**ADVANCE INFORMATION**

**BCD INPUT PLL  
FREQUENCY SYNTHESIZER**

This is one of a family of LSI PLL frequency synthesizer parts from MOTOROLA CMOS. The family includes devices having serial, parallel, 4-bit data bus and BCD programmable inputs.

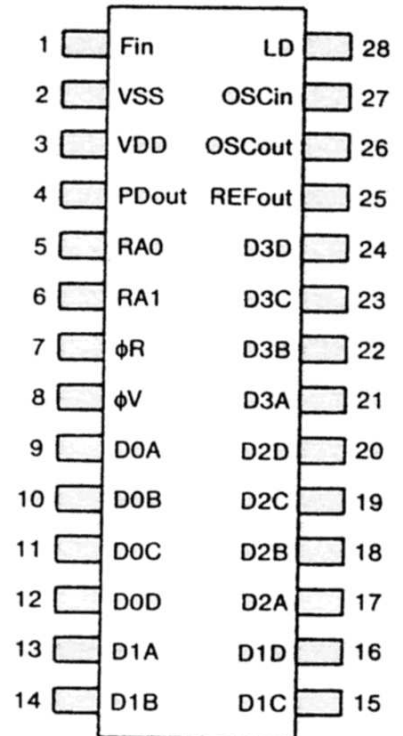
This is programmed by 4 digit BCD inputs. The device features consist of a reference oscillator, selectable reference divider, two output phase detectors and a 4 digit BCD programmable divided-by-N counter.

- General Purpose Applications
  - Two-Way Radio
  - Amateur Radio
  - Industrial Receiver
- Low Power Consumption
- 3.0 to 9.0 Vdc Supply Range
- > 30 MHz Typical Input Capability @ 5 Vdc
- On or Off - Chip Reference Oscillator Operation
- Lock Detect Signal
- 4 User - Selectable  $\div R$  Value - 512, 1024, 2048, 4096
- $\div N$  Range = 3 to 9999
- 'Linearized' Digital Phase Detector Enhances Transfer Function linearity
- Two Error Signal Options: Single Ended (Three-State) Double Ended

C SUFFIX  
PLASTIC  
QUAD PACKAGE

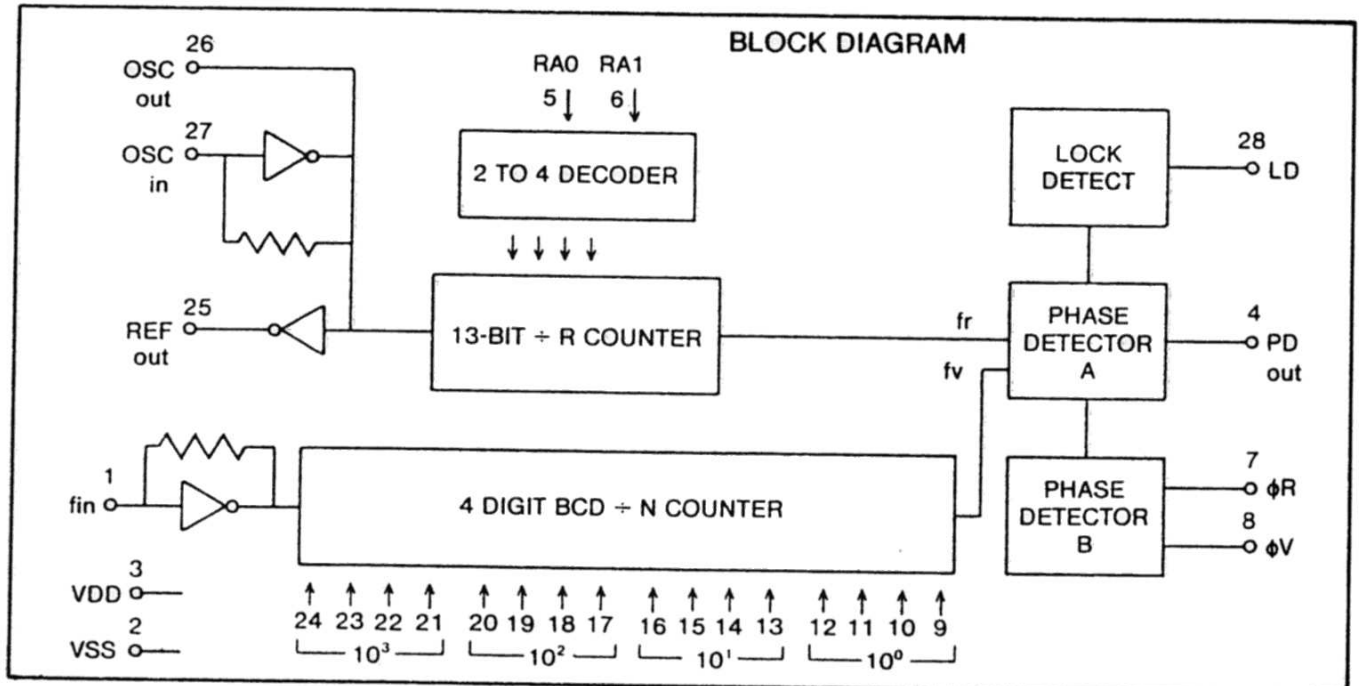
P SUFFIX  
PLASTIC  
DIL PACKAGE  
CASE 710

**PIN ASSIGNMENT (P SUFFIX)**



5

**BLOCK DIAGRAM**





## PHASE COMPARATOR AND PROGRAMMABLE COUNTERS

The MC14568B consists of a phase comparator, a divide-by-4, 16, 64 or 100 counter and a programmable divide-by-N 4-bit binary counter (all positive-edge triggered) constructed with MOS P-channel and N-channel enhancement mode devices (complementary MOS) in a single monolithic structure.

The MC14568B has been designed for use in conjunction with a programmable divide-by-N counter for frequency synthesizers and phase-locked loop applications requiring low power dissipation and/or high noise immunity.

This device can be used with both counters cascaded and the output of the second counter connected to the phase comparator (CTL high), or used separate of the programmable divide-by-N counter, for example cascaded with MC14569B (CTL low), MC14522B or MC14526B.

- Quiescent Current = 5.0 nA typ/pkg @ 5 Vdc
- Supply Voltage Range = 3.0 Vdc to 18 Vdc
- Capable of Driving Two Low-Power TTL Loads, One Low-Power Schottky TTL Load or Two HTL Loads Over the Rated Temperature Range.

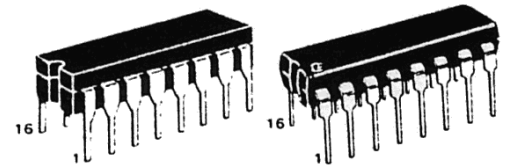
### MAXIMUM RATINGS (Voltages referenced to V<sub>SS</sub>)

Rating	Symbol	Value	Unit
Supply Voltage	V <sub>DD</sub>	-0.5 to +18	Vdc
Output Voltage, All Inputs	V <sub>in</sub>	-0.5 to V <sub>DD</sub> + 0.5	Vdc
Current Drain per Pin	I	10	mAdc
Operating Temperature Range - AL Device	T <sub>A</sub>	-55 to +125	°C
Operating Temperature Range - CL/CP Device	T <sub>A</sub>	-40 to +85	°C
Storage Temperature Range	T <sub>stg</sub>	-65 to +150	°C

## McMOS MSI

(LOW-POWER COMPLEMENTARY MOS)

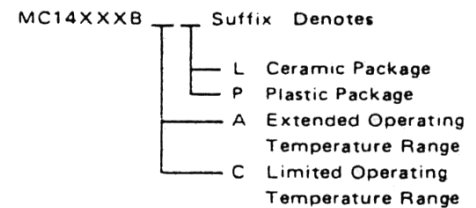
## PHASE COMPARATOR AND PROGRAMMABLE COUNTERS



**L SUFFIX**  
CERAMIC PACKAGE  
CASE 620

**P SUFFIX**  
PLASTIC PACKAGE  
CASE 648

### ORDERING INFORMATION



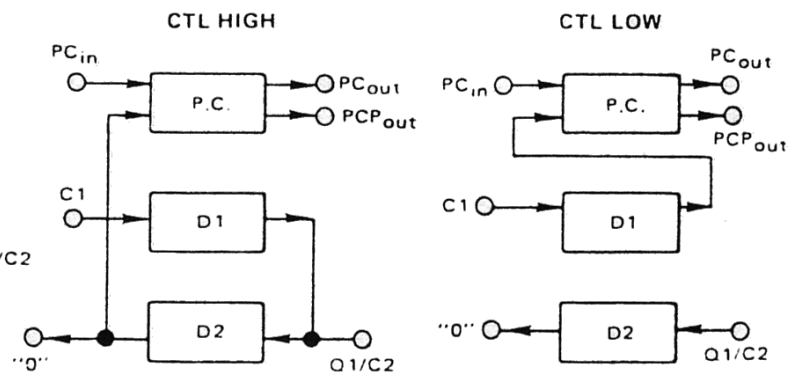
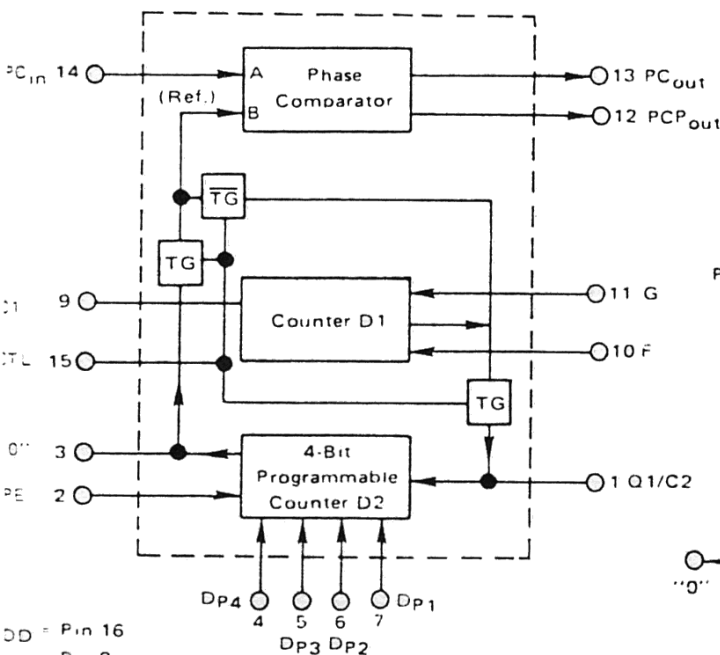
5

### TRUTH TABLE

F Pin 10	G Pin 11	Division Ratio of Counter D1
0	0	4
0	1	16
1	0	64
1	1	100

The divide-by-zero state on the programmable divide-by-N 4-bit binary counter, D2, is illegal.

### BLOCK DIAGRAM



**ORDERING INFORMATION**

Device	Temperature Range	Package
MC1496G	0°C to +70°C	Metal Can
MC1496L	0°C to +70°C	Ceramic DIP
MC1496P	0°C to +70°C	Plastic DIP
MC1596G	-55°C to +125°C	Metal Can
MC1596L	-55°C to +125°C	Ceramic DIP

**Specifications and Applications Information**

**BALANCED MODULATOR – DEMODULATOR**

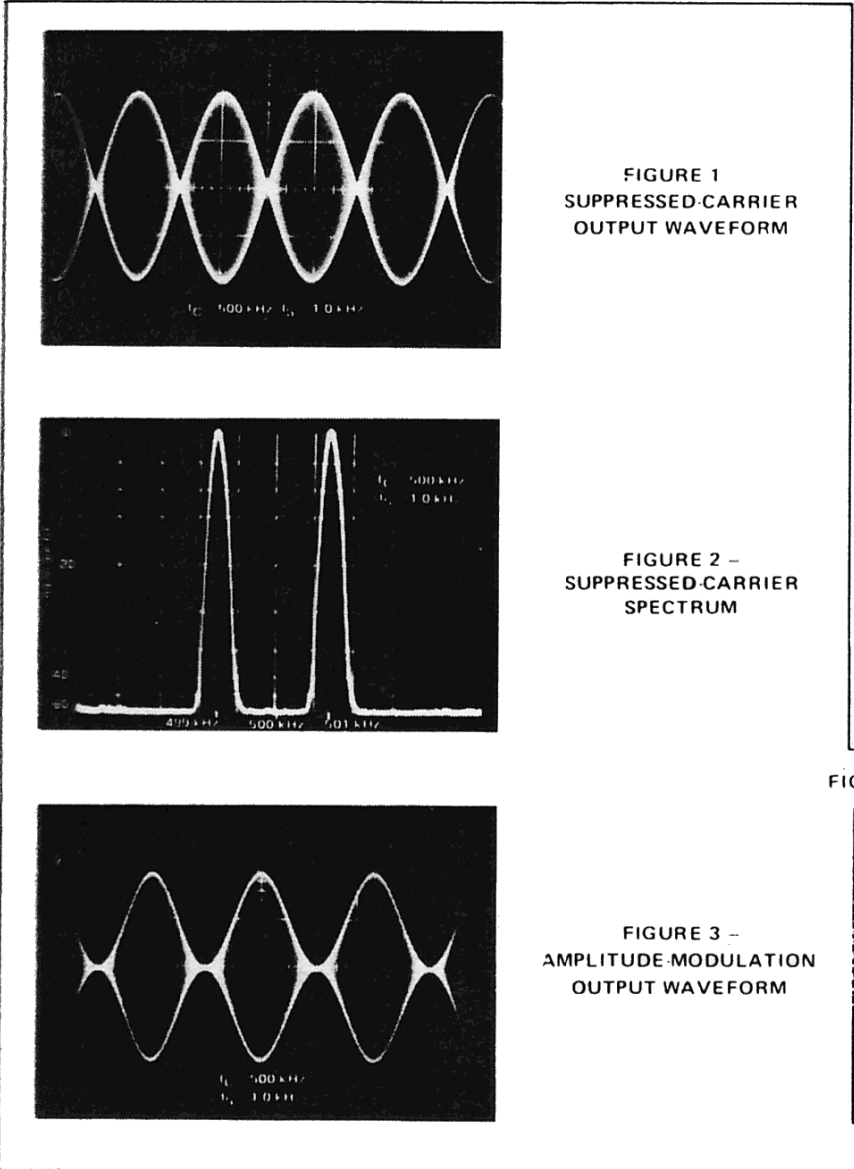
... designed for use where the output voltage is a product of an input voltage (signal) and a switching function (carrier). Typical applications include suppressed carrier and amplitude modulation, synchronous detection, FM detection, phase detection, and chopper applications. See Motorola Application Note AN-531 for additional design information.

- Excellent Carrier Suppression – 65 dB typ @ 0.5 MHz  
– 50 dB typ @ 10 MHz
- Adjustable Gain and Signal Handling
- Balanced Inputs and Outputs
- High Common-Mode Rejection – 85 dB typ

**MC1496  
MC1596**

**BALANCED MODULATOR – DEMODULATOR**

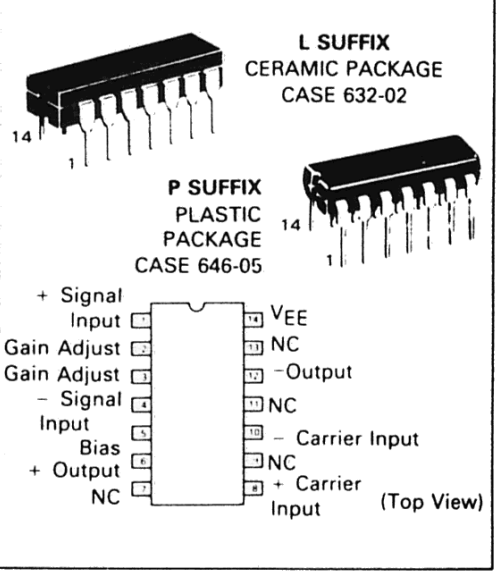
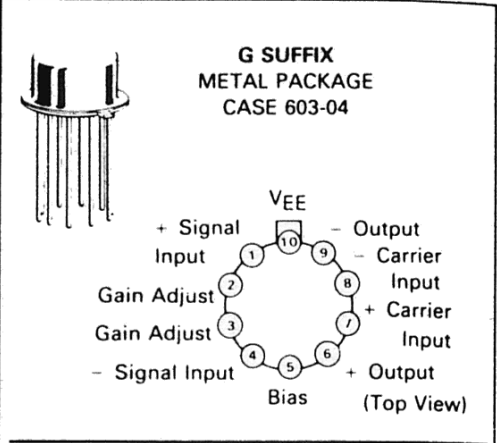
**SILICON MONOLITHIC INTEGRATED CIRCUIT**



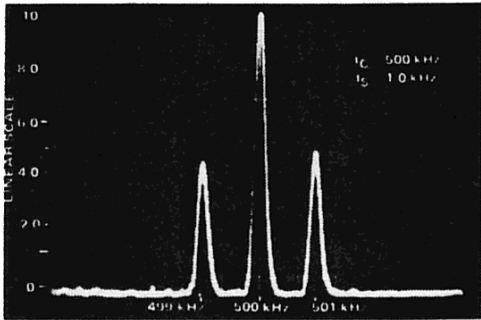
**FIGURE 1  
SUPPRESSED-CARRIER  
OUTPUT WAVEFORM**

**FIGURE 2 –  
SUPPRESSED-CARRIER  
SPECTRUM**

**FIGURE 3 –  
AMPLITUDE-MODULATION  
OUTPUT WAVEFORM**



**FIGURE 4 – AMPLITUDE-MODULATION SPECTRUM**



5



## Advance Information

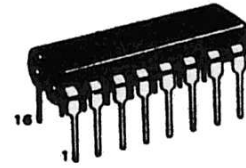
### LOW POWER FM TRANSMITTER SYSTEM

MC2831A is one chip FM transmitter system designed for cordless phone and FM communication equipments. It includes Mic Amplifier, Pilot Tone Oscillator, Voltage Controlled Oscillator and Battery Checker.

- Wide range of operating supply voltage (3.0V–8.0V)
- Low drain current (4.0mA typ full operation at  $V_{CC} = 4.0V$ )
- Battery checker (290  $\mu A$  typ at  $V_{CC} = 4.0V$ )
- Low number of external parts required

### LOW POWER FM TRANSMITTER SYSTEM

### SILICON MONOLITHIC INTEGRATED CIRCUIT

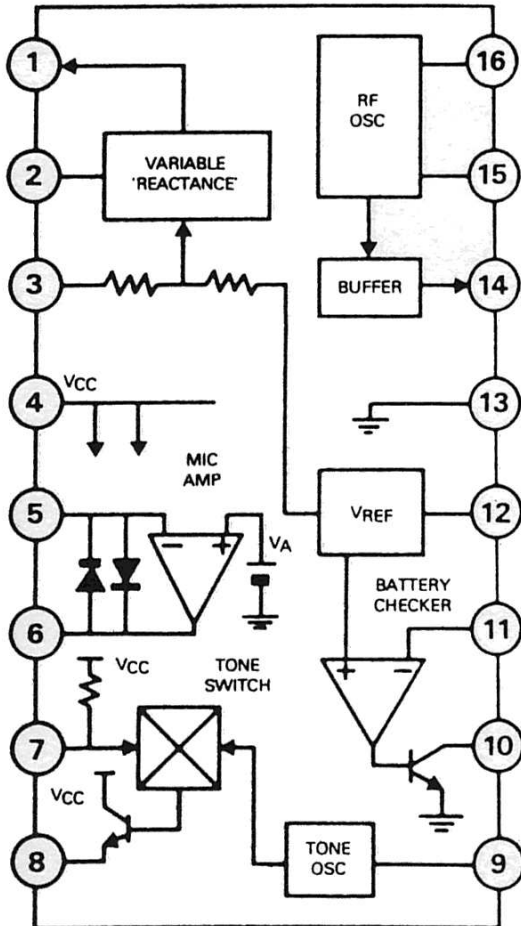


P SUFFIX  
PLASTIC PACKAGE  
CASE 648

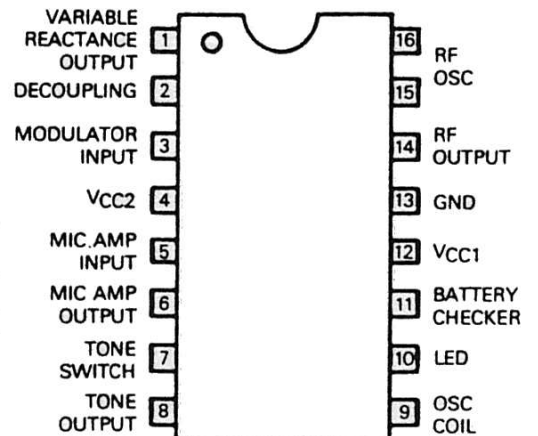


D SUFFIX  
SOIC  
CASE 751 B

FIGURE 1 — FUNCTIONAL BLOCK DIAGRAM



### PIN CONNECTIONS



## Advance Information

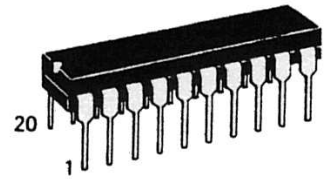
### WIDEBAND FSK RECEIVER

... includes Oscillator, Mixer, Limiting IF Amplifier, Quadrature Detector, Audio Buffer, Squelch, Meter Drive, Squelch Status output, and Data Shaper comparator. The MC3356 is designed for use in digital data communications equipment.

- Data Rates up to 500 kilobaud
- Excellent Sensitivity:  $-3$  dB Limiting Sensitivity  
 $30 \mu\text{Vrms}$  @  $100$  MHz
- Highly versatile, full-function device, yet few external parts are required

### WIDEBAND FSK RECEIVER

MONOLITHIC SILICON  
INTEGRATED CIRCUIT



**P SUFFIX**  
PLASTIC PACKAGE  
CASE 738

FIGURE 1 — FUNCTIONAL BLOCK DIAGRAM

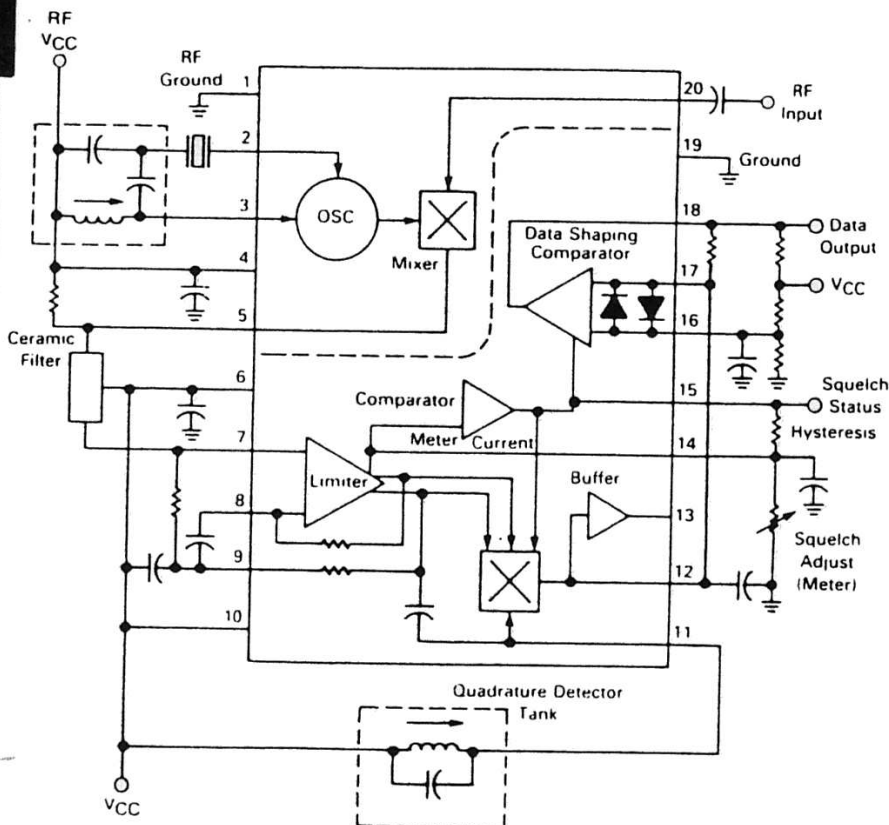
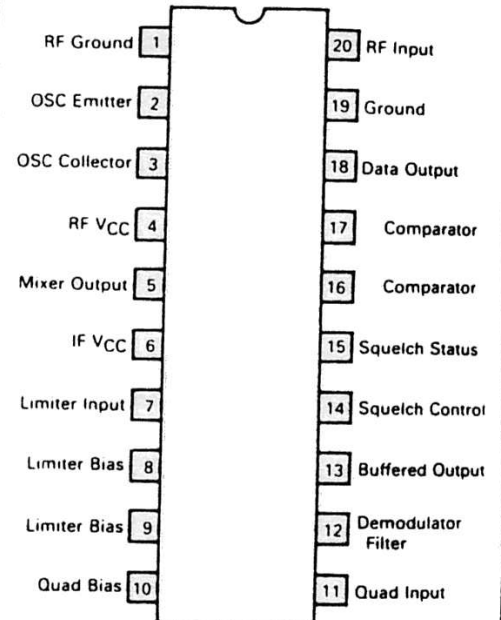


FIGURE 2 — PIN CONNECTIONS

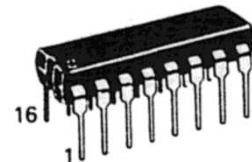


5

**LOW POWER NARROW BAND FM IF**

... includes Oscillator, Mixer, Limiting Amplifier, Quadrature Discriminator, Active Filter, Squelch, Scan Control, and Mute Switch. The MC3357 is designed for use in FM dual conversion communications equipment.

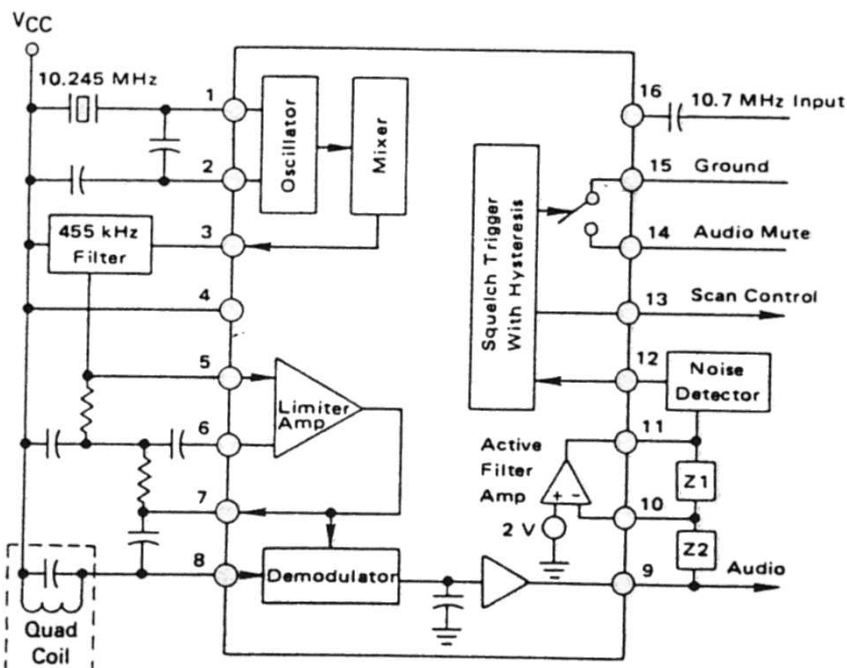
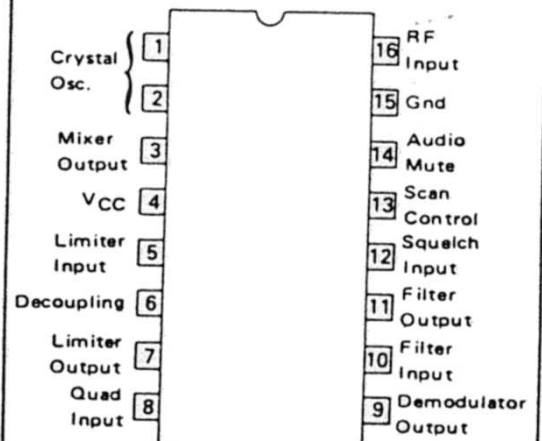
- Low Drain Current (3.0 mA (Typ) @  $V_{CC} = 6.0$  Vdc)
- Excellent Sensitivity: Input Limiting Voltage – (-3.0 dB) = 5.0  $\mu$ V (Typ)
- Low Number of External Parts Required

**LOW POWER  
FM IF**
**SILICON MONOLITHIC  
INTEGRATED CIRCUIT**


**P SUFFIX  
PLASTIC PACKAGE  
CASE 648-05**



**D SUFFIX  
PLASTIC PACKAGE  
CASE 751B-01  
SO-16**

**FIGURE 1 — FUNCTIONAL BLOCK DIAGRAM**

**PIN CONNECTIONS**




## Advance Information

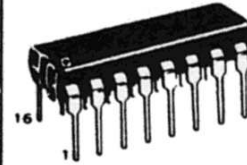
### LOW POWER NARROW BAND FM IF

... includes Oscillator, Mixer, Limiting Amplifier, Quadrature Discriminator, Active Filter, Squelch, Scan Control, and Mute Switch. The MC3361A is designed for use in FM dual conversion communications equipment.

- Operates From 2.0 V to 8.0 V Supply
- Low Drain Current 4.2 mA Typ @  $V_{CC} = 4.0$  Vdc
- Excellent Sensitivity: Input Limiting Voltage—  
-3.0 dB = 2.0  $\mu$ V Typ
- Low Number of External Parts Required
- Operating Frequency Up to 60 MHz

### LOW POWER FM IF

### SILICON MONOLITHIC INTEGRATED CIRCUIT



**P SUFFIX**  
PLASTIC PACKAGE  
CASE 648-05

**D SUFFIX**  
SOIC  
CASE 751B

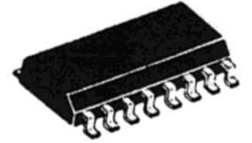
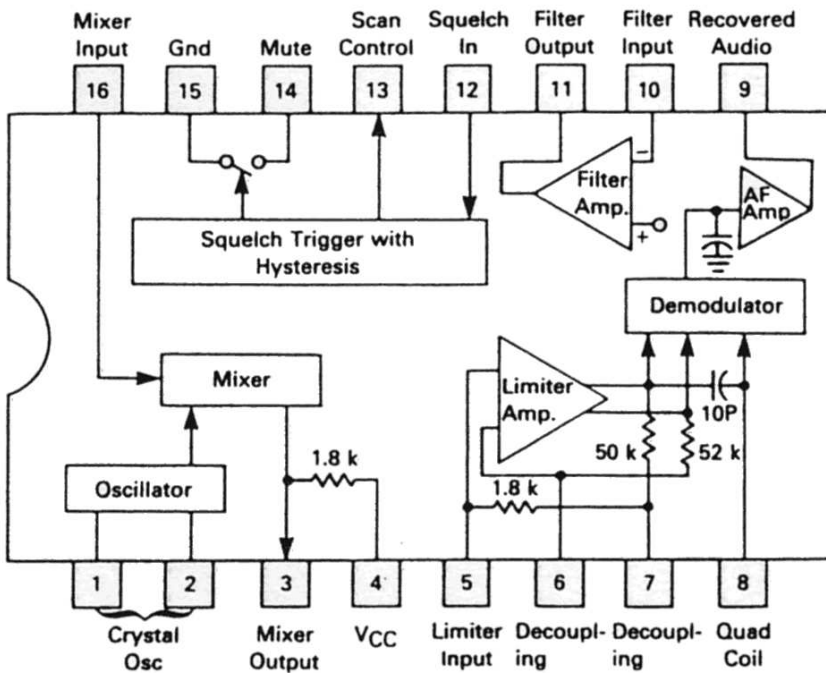
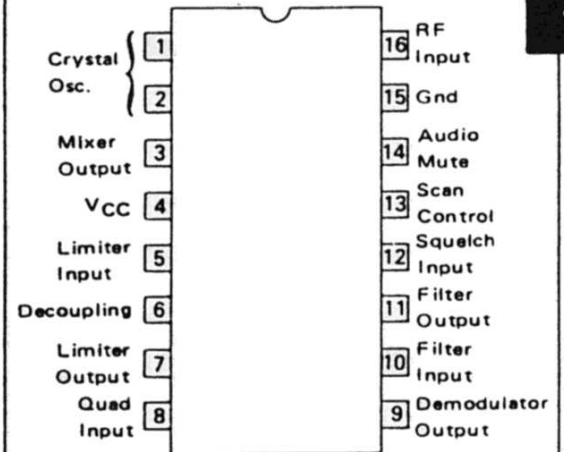


FIGURE 1 — FUNCTIONAL BLOCK DIAGRAM



PIN CONNECTIONS







**MOTOROLA**

**MC3362/63**

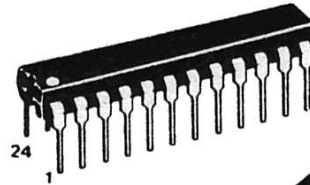
**Product Preview**

**RECEIVER I.C.**

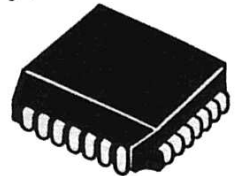
**FEATURES**

- Single Supply Operation from 2-7 VDC
- Low Power Consumption (3mA at 2 V Typ)
- RF Input Frequency Response to over 50 MHz at  $V_{CC} = 2 V$
- Doubly Balanced First Mixer
- First LO configurable as XCO or VCO with On Board Tuning Diodes
- Wide Dynamic Range Signal Strength Indicator with Externally Set Threshold
- Data Slicer detects Zero Crossings of FSK Modulation of Carrier
- Available in Full Function 28 Pin Quad (Surface Mount) or 24 Pin DIN Packages

**PACKAGING & PIN OUT\***

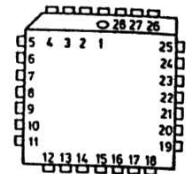
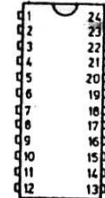


P SUFFIX  
PLASTIC PACKAGE  
CASE 724-02



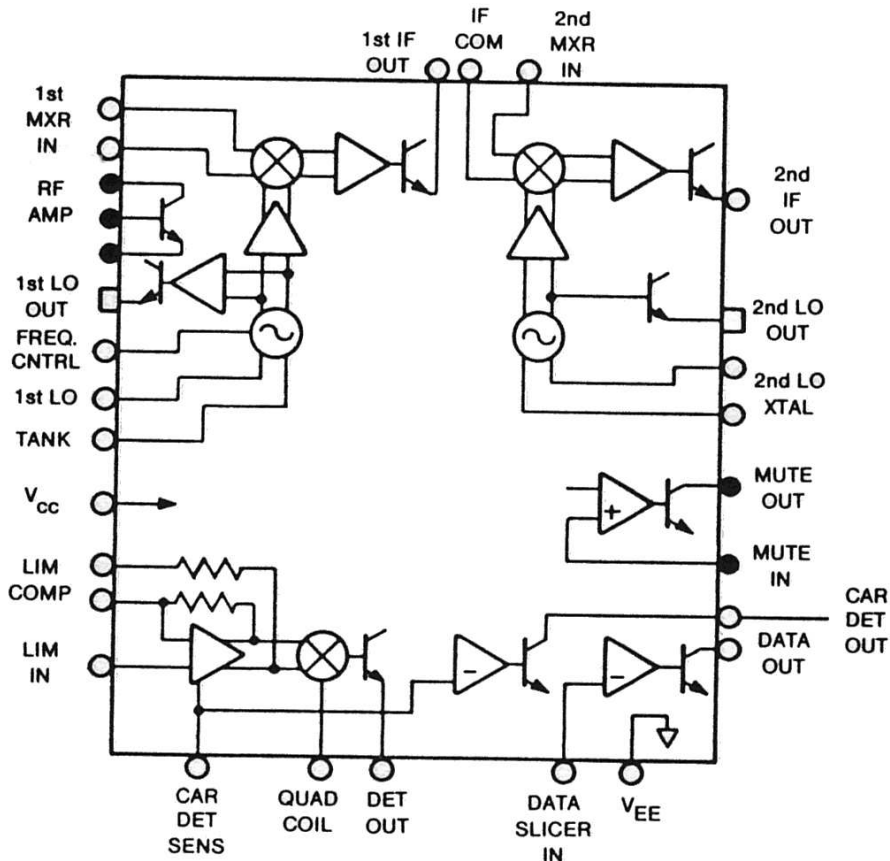
PLASTIC QUAD  
SURFACE MOUNT  
CASE 776-01

MC3362



MC3363

**MC3362/63 RECEIVER I.C.  
INTERNAL BLOCK DIAGRAM**



**PIN OPTIONS**

- ONLY AVAILABLE ON 24 PIN DIP, MC3362
- ONLY AVAILABLE ON 28 PIN QUAD, MC3363

5





**MOTOROLA**

**MC3393P**

**Advance Information**

**TWO MODULUS PRESCALER**

The MC3393P can divide by 15 and 16, and can be used with Motorola CMOS frequency synthesizers MC145146, 52, 56 for commercial AM-FM radio, land mobile and marine two-way radios, avionic radios, and scanner receivers.

- 140 MHz (typ) Toggle Frequency
- $\div 15/16$
- TTL and CMOS Compatible Output
- Active Pullup and Pulldown
- +5.0 V Supply
- Buffered Clock Input
- 100-400 mV (typ) Input Sensitivity
- 200 Milliwatts (typ)

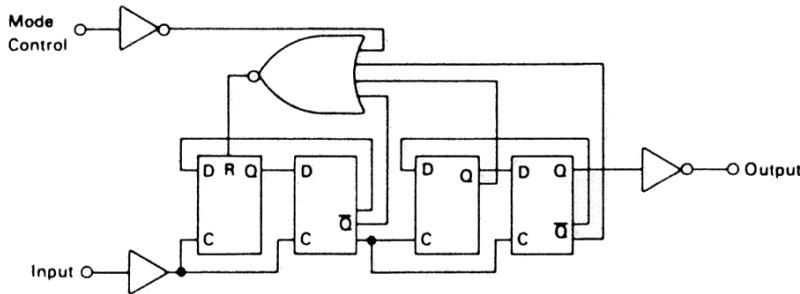
**TWO MODULUS PRESCALER**

**SILICON MONOLITHIC INTEGRATED CIRCUIT**

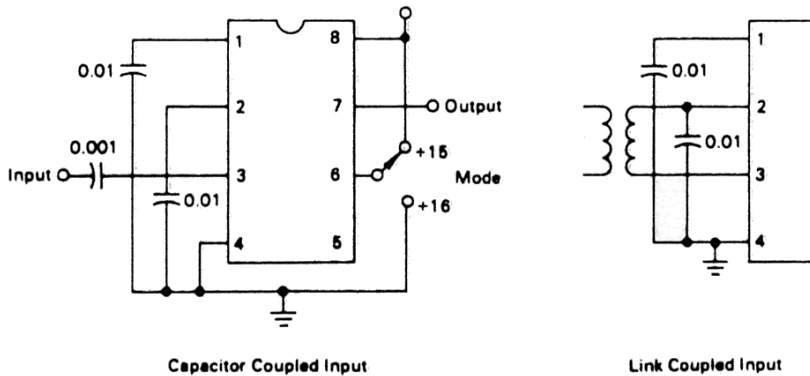


**N SUFFIX  
PLASTIC PACKAGE  
CASE 626-04**

**FIGURE 1 — LOGIC DIAGRAM**



**FIGURE 2 — TEST CIRCUITS**



- Pin Outs**
1. Bias Decouple
  2. Bias Decouple
  3. Input
  4. Ground
  5. NC
  6. Input
  7. Output
  8. V<sub>CC</sub>

**5**

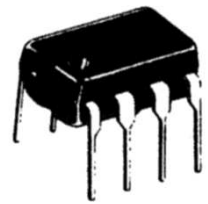
**Advance Information**
**DIVIDE BY 20 PRESCALER**

The MC3396P is a fixed  $\div 20$  prescaler for use in frequency synthesizers and similar applications.

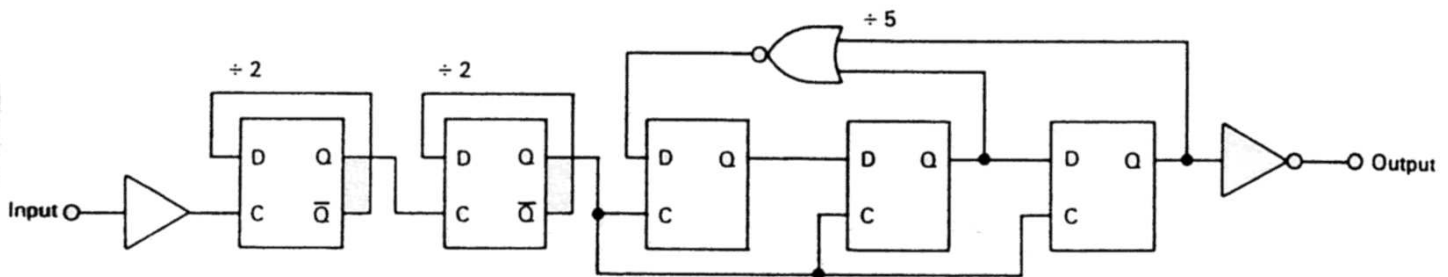
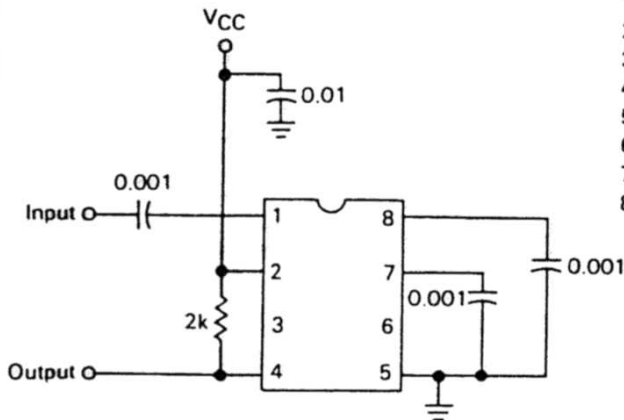
- 200 MHz (typ) Toggle Frequency
- Single 5.0 Volt Supply
- Buffered Clock Input
- 100 mV — 400 mV RMS Input Sensitivity
- Open Collector Saturating Output is Capable of Driving TTL and CMOS.

**DIVIDE BY 20  
PRESCALER**

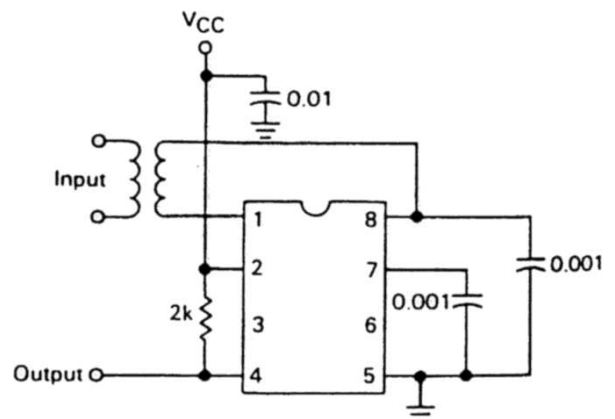
SILICON MONOLITHIC  
INTEGRATED CIRCUIT



P SUFFIX  
PLASTIC PACKAGE  
CASE 626

**FIGURE 1 — LOGIC DIAGRAM**

**FIGURE 2 — CAPACITOR-COUPLED INPUT**

**PIN CONNECTIONS**

1. Input
2. VCC
3. NC
4. Output
5. Ground
6. NC
7. Bias Decouple
8. Bias Decouple

**FIGURE 3 — LINK-COUPLED INPUT**




**MOTOROLA**

**PROGRAMMABLE MODULO-N  
COUNTERS**

The monolithic devices are programmable, cascadable, modulo-N-counters. The MC4316/4016 can be programmed to divide by any number (N) from 0 thru 9, the MC4318/4018 from 0 thru 15. The MC4317/4017 consists of a modulo 2 counter which can be programmed to divide by 0 or 1 and a modulo 5 counter which can be programmed to divide by any number from 0 to 4. The MC4319/4019 contains two modulo 4 counters, which can be programmed to divide by any number from 0 to 3.

The parallel enable (PE) input enables the parallel data inputs D0 thru D3. All zeros are entered into the counter by applying a logic "0" level to the master reset (MR) and PE inputs. This causes the counter to stop counting (count = 0). All data inputs are independent of the logic level of the Clock.

Modulo-N counters are useful in frequency synthesizers, in phase-locked loops, and in other applications where a simple method for frequency division is needed.

**All Types:**

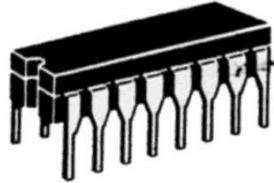
Input Loading Factor:      Total Power Dissipation =  
 Clock, PE = 2                      250 mW typ/pkg  
 D0, D1, D2, D3, Gate = 1      Propagation Delay Time:  
 MR = 4                              Clock to Q3 = 50 ns typ  
 Output Loading Factor = 8        Clock to Bus = 35 ns typ

**MC4316 • MC4016**

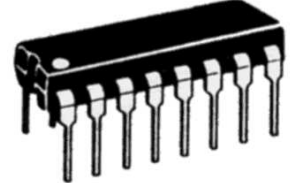
**MC4317 • MC4017**

**MC4318 • MC4018**

**MC4319 • MC4019**

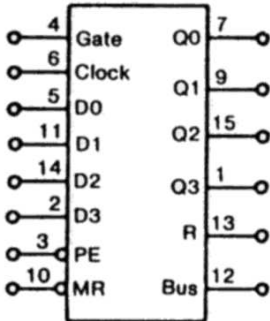


**L SUFFIX  
CERAMIC PACKAGE  
CASE 620**



**P SUFFIX  
PLASTIC PACKAGE  
CASE 648  
MC4016 thru MC4019  
only**

**MC4316/4016  
MC4318/4018**



V<sub>CC</sub> = Pin 16  
Gnd = Pin 8

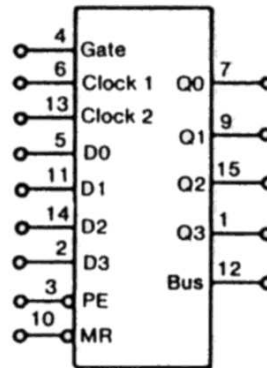
**MC4318/4018**

COUNT	OUTPUT			
	Q3	Q2	Q1	Q0
15	1	1	1	1
14	1	1	1	0
13	1	1	0	1
12	1	1	0	0
11	1	0	1	1
10	1	0	1	0
9	1	0	0	1
8	1	0	0	0
7	0	1	1	1
6	0	1	1	0
5	0	1	0	1
4	0	1	0	0
3	0	0	1	1
2	0	0	1	0
1	0	0	0	1
0	0	0	0	0

**MC4316/4016**

COUNT	OUTPUT			
	Q3	Q2	Q1	Q0
9	1	0	0	1
8	1	0	0	0
7	0	1	1	1
6	0	1	1	0
5	0	1	0	1
4	0	1	0	0
3	0	0	1	1
2	0	0	1	0
1	0	0	0	1
0	0	0	0	0

**MC4317/4017  
MC4319/4019**



V<sub>CC</sub> = Pin 16  
Gnd = Pin 8

**MC4317/4017**

COUNT	OUTPUT
	Q0
1	1
0	0

**MC4319/4019**

COUNT	OUTPUT	
	Q1	Q0
3	1	1
2	1	0
1	0	1
0	0	0

COUNT	OUTPUT		
	Q3	Q2	Q1
4	1	0	0
3	0	1	1
2	0	1	0
1	0	0	1
0	0	0	0

COUNT	OUTPUT	
	Q3	Q2
3	1	1
2	1	0
1	0	1
0	0	0



# **Phase Locked Loop Design Fundamentals (AN535)**

**Phase-Locked Loop**

**6**



## INTRODUCTION

The purpose of this application note is to provide the electronic system designer with the necessary tools to design and evaluate Phase Locked Loops (PLL) configured with integrated circuits. The majority of all PLL design problems can be approached using the Laplace transform technique. Therefore, a brief review of Laplace is included to establish a common reference with the reader. Since the scope of this article is practical in nature all theoretical derivations have been omitted hoping to simplify and clarify the content. A bibliography is included for those who desire to pursue the theoretical aspect.

## PARAMETER DEFINITION

The Laplace Transform permits the representation of a time response  $f(t)$  of a system in the complex domain ( $s$ ). This response is twofold in nature in that it contains both the transient and steady state solutions. Thus, all operating conditions are considered and evaluated. The Laplace transform is valid only for positive real time linear parameters; thus, its use must be justified for the PLL which includes both linear and nonlinear functions. This justification is presented in Chapter Three of Phase Lock Techniques by Gardner.<sup>1</sup>

The parameters in Figure 1 are defined and will be used throughout the text.

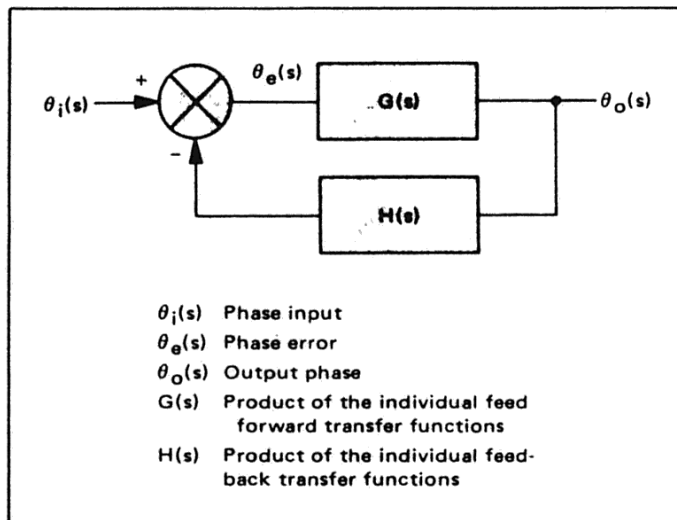


FIGURE 1 – Feedback System

Using servo theory, the following relationships can be obtained.<sup>2</sup>

$$\theta_e(s) = \frac{1}{1 + G(s)H(s)} \theta_i(s) \quad (1)$$

$$\theta_o(s) = \frac{G(s)}{1 + G(s)H(s)} \theta_i(s) \quad (2)$$

These parameters relate to the functions of a PLL as shown in Figure 2.

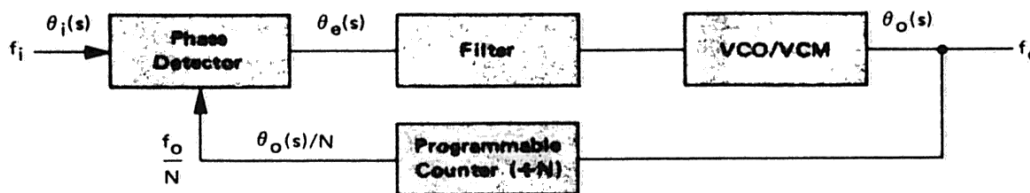


FIGURE 2 – Phase Locked Loop

Circuit diagrams external to Motorola products are included as a means of illustrating typical semiconductor applications; consequently, complete information sufficient for construction purposes is not necessarily given. The information in this Application Note has been carefully checked and is believed to be entirely reliable. However, no responsibility is assumed for inaccuracies. Furthermore, such information does not convey to the purchaser of the semiconductor devices described any license under the patent rights of Motorola Inc. or others.

The phase detector produces a voltage proportional to the phase difference between the signals  $\theta_i$  and  $\theta_o/N$ . This voltage upon filtering is used as the control signal for the VCO/VCM (VCM - Voltage Controlled Multivibrator).

Since the VCO/VCM produces a frequency proportional to its input voltage, any time variant signal appearing on the control signal will frequency modulate the VCO/VCM. The output frequency is

$$f_o = N f_i \quad (3)$$

during phase lock. The phase detector, filter, and VCO/VCM compose the feed forward path with the feedback path containing the programmable divider. Removal of the programmable counter produces unity gain in the feedback path ( $N = 1$ ). As a result, the output frequency is then equal to that of the input.

Various types and orders of loops can be constructed depending upon the configuration of the overall loop transfer function. Identification and examples of these loops are contained in the following two sections.

### TYPE - ORDER

These two terms are used somewhat indiscriminately in published literature, and to date there has not been an established standard. However, the most common usage will be identified and used in this article.

The type of a system refers to the number of poles of the loop transfer function  $G(s) H(s)$  located at the origin. Example:

$$\text{let } G(s) H(s) = \frac{10}{s(s+10)} \quad (4)$$

This is a type one system since there is only one pole at the origin.

The order of a system refers to the highest degree of the polynomial expression

$$1 + G(s) H(s) = 0 \triangleq \text{C.E.} \quad (5)$$

which is termed the Characteristic Equation (C.E.). The roots of the characteristic equation become the closed loop poles of the overall transfer function.

Example:

$$G(s) H(s) = \frac{10}{s(s+10)} \quad (6)$$

then

$$1 + G(s) H(s) = 1 + \frac{10}{s(s+10)} = 0 \quad (7)$$

therefore

$$\text{C.E.} = s(s+10) + 10 \quad (8)$$

$$\text{C.E.} = s^2 + 10s + 10 \quad (9)$$

which is a second order polynomial. Thus, for the given  $G(s) H(s)$ , we obtain a type 1 second order system.

### ERROR INSTANT

Various inputs can be applied to a system. Typically these include step position, velocity, and acceleration. The response of type 1, 2, and 3 systems will be examined with the various inputs.

$\theta_e(s)$  represents the phase error that exists in the phase detector between the incoming reference signal  $\theta_i(s)$  and the feedback  $\theta_o(s)/N$ . In evaluating a system,  $\theta_e(s)$  must be examined in order to determine if the steady state and transient characteristics are optimum and/or satisfactory. The transient response is a function of loop stability and is covered in the next section. The steady state evaluation can be simplified with the use of the final value theorem associated with Laplace. This theorem permits finding the steady state system error  $\theta_e(s)$  resulting from the input  $\theta_i(s)$  without transforming back to the time domain.<sup>3</sup>

Simply stated

$$\lim_{t \rightarrow \infty} [\theta(t)] = \lim_{s \rightarrow 0} [s \theta_e(s)] \quad (10)$$

Where

$$\theta_e(s) = \frac{1}{1 + G(s) H(s)} \theta_i(s) \quad (11)$$

The input signal  $\theta_i(s)$  is characterized as follows:

$$\text{Step position: } \theta_i(t) = C_p \quad t \geq 0 \quad (12)$$

$$\text{Or, in Laplace notation: } \theta_i(s) = \frac{C_p}{s} \quad (13)$$

where  $C_p$  is the magnitude of the phase step in radians. This corresponds to shifting the phase of the incoming reference signal by  $C_p$  radians:

$$\text{Step velocity: } \theta_i(t) = C_v t \quad t \geq 0 \quad (14)$$

$$\text{Or, in Laplace notation: } \theta_i(s) = \frac{C_v}{s^2} \quad (15)$$

where  $C_v$  is the magnitude of the rate of change of phase in radians per second. This corresponds to inputting a frequency that is different than the feedback portion of the VCO frequency. Thus,  $C_v$  is the frequency difference in radians per second seen at the phase detector.

$$\text{Step acceleration: } \theta_i(t) = C_a t^2 \quad t \geq 0 \quad (16)$$

$$\text{Or, in Laplace notation: } \theta_i(s) = \frac{2 C_a}{s^3} \quad (17)$$

$C_a$  is the magnitude of the frequency rate of change in radians per second per second. This is characterized by a time variant frequency input.

Typical loop  $G(s) H(s)$  transfer functions for types 1, 2, and 3 are:

$$\text{Type 1 } G(s) H(s) = \frac{K}{s(s+a)} \quad (18)$$



$$\text{Type 2 } G(s)H(s) = \frac{K(s+a)}{s^2} \quad (19)$$

$$\text{Type 3 } G(s)H(s) = \frac{K(s+a)(s+b)}{s^3} \quad (20)$$

The final value of the phase error for a type 1 system with a step phase input is found by using Equations 11 and 13.

$$\begin{aligned} \theta_e(s) &= \left( \frac{1}{1 + \frac{K}{s(s+a)}} \right) \left( \frac{C_p}{s} \right) \\ &= \frac{(s+a)C_p}{(s^2 + as + K)} \end{aligned} \quad (21)$$

$$\theta_e(t=\infty) = \lim_{s \rightarrow 0} \left[ s \left( \frac{s+a}{s^2 + as + K} \right) C_p \right] = 0 \quad (22)$$

Thus the final value of the phase error is zero when a step position (phase) is applied.

Similarly applying the three inputs into type 1, 2 and 3 systems and utilizing the final value theorem, the following table can be constructed showing the respective steady state phase errors.

TABLE I – Steady State Phase Errors for Various System Types

	Type 1	Type 2	Type 3
Step Position	Zero	Zero	Zero
Step Velocity	Constant	Zero	Zero
Step Acceleration	Continually Increasing	Constant	Zero

A zero phase error identifies phase coherence between two input signals at the phase detector.

A constant phase error identifies a phase differential between the two input signals at the phase detector. The magnitude of this differential phase error is proportional to loop gain and the magnitude of the input step.

A continually increasing phase error identifies a time change of phase. This is an unlocked condition for a phase loop.

Using Table I the system type can be determined for specific inputs. For instance, if it is desired for a PLL to track a reference frequency (step velocity) with zero phase error, a minimum of type 2 is required.

#### STABILITY

The root locus technique of determining the position of system poles and zeroes in the s-plane is often used to graphically visualize the system stability. The graph or plot illustrates how the closed loop poles (roots of the character-

istic equation) vary with loop gain. For stability all poles must lie in the left half of the s-plane. The relationship of the system poles and zeroes then determine the degree of stability. The root locus contour can be determined by using the following guidelines.<sup>2</sup>

Rule 1 - The root locus begins at the poles of  $G(s)H(s)$  ( $K = 0$ ) and ends at the zeroes of  $G(s)H(s)$  ( $K = \infty$ ). Where  $K$  is loop gain.

Rule 2 - The number of root loci branches is equal to the number of poles or number of zeroes, whichever is greater. The number of zeroes at infinity is the difference between the number of finite poles and finite zeroes of  $G(s)H(s)$ .

Rule 3 - The root locus contour is bounded by asymptotes whose angular position is given by

$$\frac{(2n+1)}{\#P - \#Z} \pi; n = 0, 1, 2, \dots \quad (23)$$

Where  $\#P$  ( $\#Z$ ) is the number of poles (zeroes).

Rule 4 - The intersection of the asymptotes is positioned at the center of gravity C. G.

$$C.G. = \frac{\Sigma P - \Sigma Z}{\#P - \#Z} \quad (24)$$

Where  $\Sigma P$  ( $\Sigma Z$ ) denotes the summation of the poles (zeroes).

Rule 5 - On a given section of the real axis, root loci may be found in the section only if the  $\#P + \#Z$  to the right is odd.

Rule 6 - Breakaway points from negative real axis is given by:

$$\frac{dK}{ds} = 0 \quad (25)$$

Again where  $K$  is the loop gain variable factored from the characteristic equation.

Example:

The root locus for a typical loop transfer function is found as follows:

$$G(s)H(s) = \frac{K}{s(s+4)} \quad (26)$$

The root locus has two branches (Rule 2) which begin at  $s = 0$  and  $s = -4$  and ends at the two zeroes located at infinity (Rule 1). The asymptotes can be found according to Rule 3. Since there are two poles and no zeroes the equation becomes:

$$\frac{2n+1}{2} \pi = \begin{cases} \frac{\pi}{2} & \text{for } n = 0 \\ \frac{3\pi}{2} & \text{for } n = 1 \end{cases} \quad (27)$$

Position the intersection according to Rule 4 is:

$$s = \frac{\Sigma P - \Sigma Z}{\#P - \#Z} = \frac{(-4 - 0) - (0)}{2 - 0}$$

$$s = -2 \quad (28)$$

The breakaway point as defined by Rule 6 can be found by first writing the characteristic equation.

$$\text{C.E.} = 1 + G(s)H(s) = 0$$

$$= 1 + \frac{K}{s(s+4)} = s^2 + 4s + K = 0 \quad (29)$$

Now solving for K yields

$$K = -s^2 - 4s \quad (30)$$

Taking the derivative with respect to s and setting it equal to zero then determines the breakaway point.

$$\frac{dK}{ds} = \frac{d}{ds} (-s^2 - 4s) \quad (31)$$

$$\frac{dK}{ds} = -2s - 4 = 0 \quad (32)$$

or

$$s = -2 \quad (33)$$

is the point of departure. Using this information, the root locus can be plotted as in Figure 3.

This second order characteristic equation given by Equation 29 has been normalized to a standard form<sup>2</sup>

$$s^2 + 2\zeta\omega_n s + \omega_n^2 \quad (34)$$

where the damping ratio  $\zeta = \cos \phi$  ( $0^\circ \leq \phi \leq 90^\circ$ ) and  $\omega_n$  is the natural frequency as shown in Figure 3.

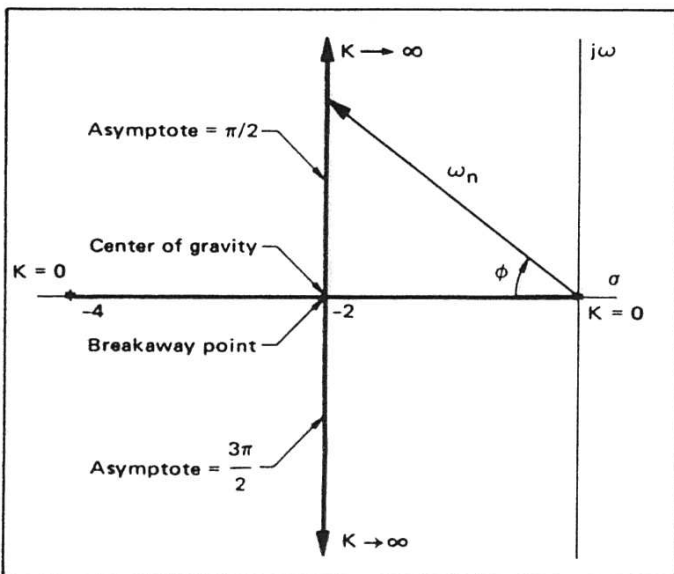


FIGURE 3 – Type 1 Second Order Root Locus Contour

The response to this type, second order system to a step input is shown in Figure 4. These curves represent the phase response to a step position (phase) input for various damping ratios. The output frequency response as a function of time to a step velocity (frequency) input is also characterized by the same set of figures.

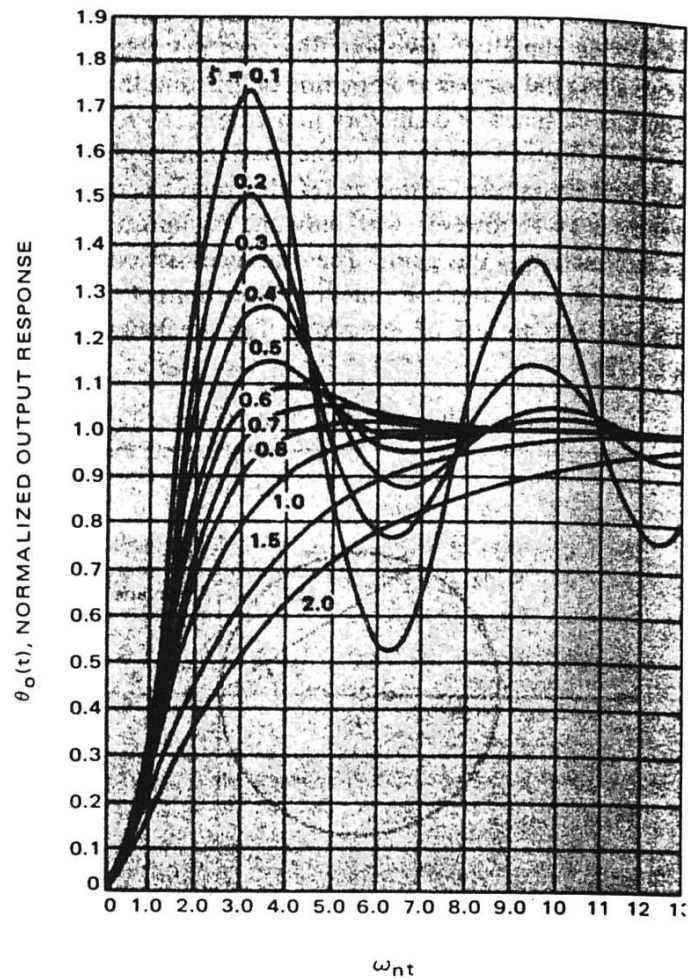


FIGURE 4 – Type 1 Second Order Step Response

The overshoot and stability as a function of the damping ratio  $\zeta$  is illustrated by the various plots. Each response is plotted as a function of the normalized time  $\omega_n t$ . For a given  $\zeta$  and a lock-up time  $t$ , the  $\omega_n$  required to achieve the desired results can be determined. Example:

$$\text{Assume } \zeta = 0.5$$

$$\text{error} < 10\%$$

$$\text{for } t > 1 \text{ ms}$$

From  $\zeta = 0.5$  curve the error is less than 10% of final value for all time greater than  $\omega_n t = 4.5$ . The required  $\omega_n$  can then be found by:

$$\omega_n t = 4.5 \quad (35)$$

or

$$\omega_n = \frac{4.5}{t} = \frac{4.5}{0.001} = 4.5 \text{ k rad/s} \quad (36)$$

$\zeta$  typically selected between 0.5 and 1 to yield optimum overshoot and noise performance.

Another common loop transfer function takes the form

$$G(s)H(s) = \frac{(s+a)k}{s^2} \quad (37)$$

This is a type 2 second order system. A zero is added to provide stability. (Without the zero the poles would move along the  $j\omega$  axis as a function of gain and the system would at all times be oscillatory in nature.) The root locus shown in Figure 5 has two branches beginning at the origin with one asymptote located at 180 degrees. The center of gravity is  $s = -a$ ; however, with only one asymptote there is no intersection at this point. The root locus lies on a circle centered at  $s = -a$  and continues on all portions of the negative real axis to left of the zero. The breakaway point is  $s = -2a$ .

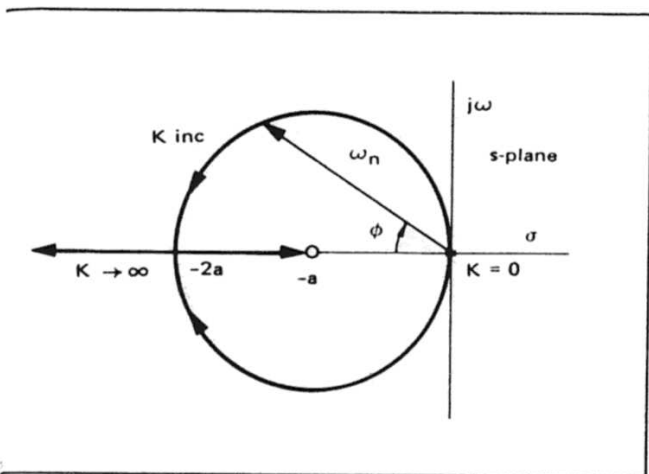


FIGURE 5 – Type 2 Second Order Root Locus Contour

The respective phase or output frequency response of this type 2 second order system to a step position (phase) or velocity (frequency) input is shown in Figure 6. As illustrated in the previous example the required  $\omega_n$  can be determined by the use of the graph when  $\zeta$  and the lock-up time are given.

### BANDWIDTH

The -3 dB bandwidth of the PLL is given by

$$\omega_{-3\text{ dB}} = \omega_n \left( 1 - 2\zeta^2 + \sqrt{2 - 4\zeta^2 + 4\zeta^4} \right)^{1/2} \quad (38)$$

for a type 1 second order system, and by

$$\omega_{-3\text{ dB}} = \omega_n \left( 1 + 2\zeta^2 + \sqrt{2 + 4\zeta^2 + 4\zeta^4} \right)^{1/2} \quad (39)$$

for a type 2 second order system.

### PHASE-LOCKED LOOP DESIGN EXAMPLE

The design of a PLL typically involves determining the type of loop required, selecting the proper bandwidth, and establishing the desired stability. A fundamental approach

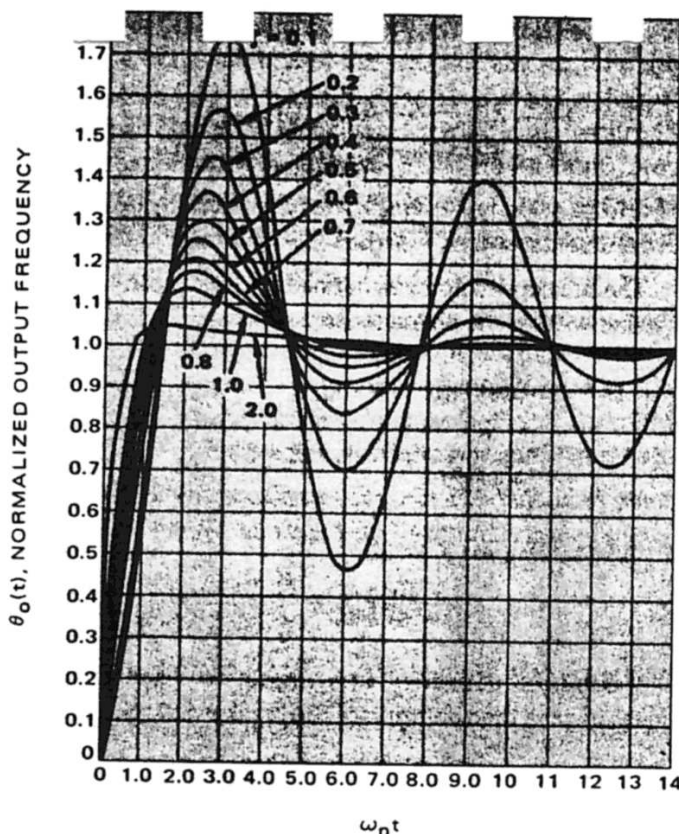


FIGURE 6 – Type 2 Second Order Step Response

to these design constraints is now illustrated. It is desired for the system to have the following specifications:

Output frequency	2.0 MHz to 3.0 MHz
Frequency steps	100 kHz
Phase coherent frequency output	—
Lock-up time between channels	1 ms
Overshoot	< 20%

NOTE: These specifications characterize a system function similar to a variable time base generator or a frequency synthesizer.

From the given specifications the circuit parameters shown in Figure 7 can now be determined.

The devices used to configure the PLL are:

Frequency-Phase Detector	MC4044/4344
Voltage Controlled Multivibrator (VCM)	MC4024/4324
Programmable Counter	MC4016/4316

The forward and feedback transfer functions are given by:

$$G(s) = K_p K_f K_o \quad H(s) = K_n \quad (40)$$

where  $K_n = 1/N$  (41)

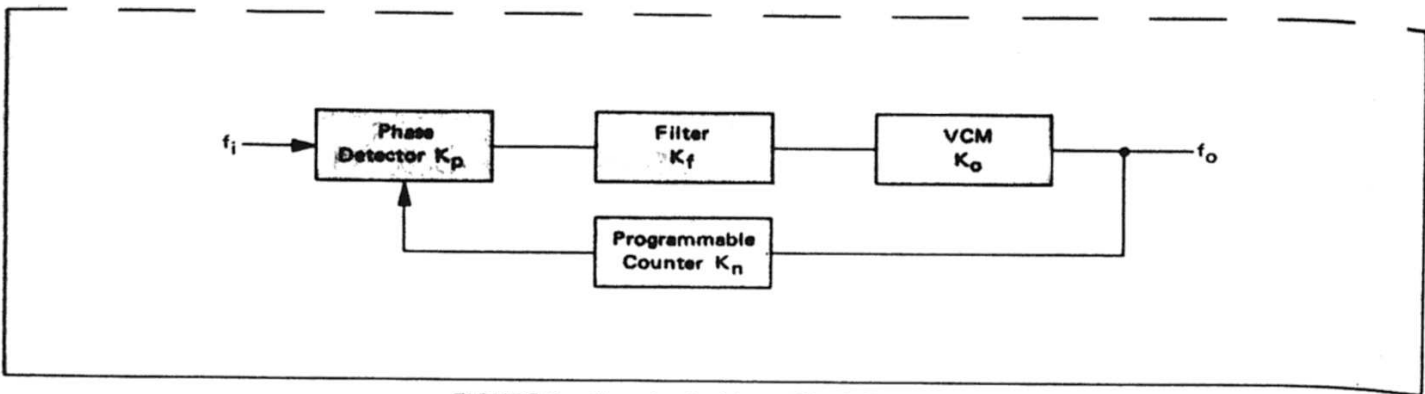


FIGURE 7 – Phase Locked Loop Circuit Parameters

The programmable counter divide ratio  $K_n$  can be found from Equation 3.

$$N_{\min} = \frac{f_o \text{ min}}{f_i} = \frac{f_o \text{ min}}{f_{\text{step}}} = \frac{2 \text{ MHz}}{100 \text{ kHz}} = 20 \quad (42)$$

$$N_{\max} = \frac{f_o \text{ max}}{f_{\text{step}}} = \frac{3 \text{ MHz}}{100 \text{ kHz}} = 30 \quad (43)$$

$$K_n = \frac{1}{20} \text{ to } \frac{1}{30} \quad (44)$$

A type 2 system is required to produce a phase coherent output relative to the input (see Table I). The root locus contour is shown in Figure 5 and the system step response is illustrated by Figure 6.

The operating range of the MC4024/4324 VCM must cover 2 MHz to 3 MHz. Selecting the VCM control capacitor according to the rules contained on the data sheet yields  $C = 100 \text{ pF}$ . The desired operating range is then centered within the total range of the device. The input voltage versus output frequency is shown in Figure 8.

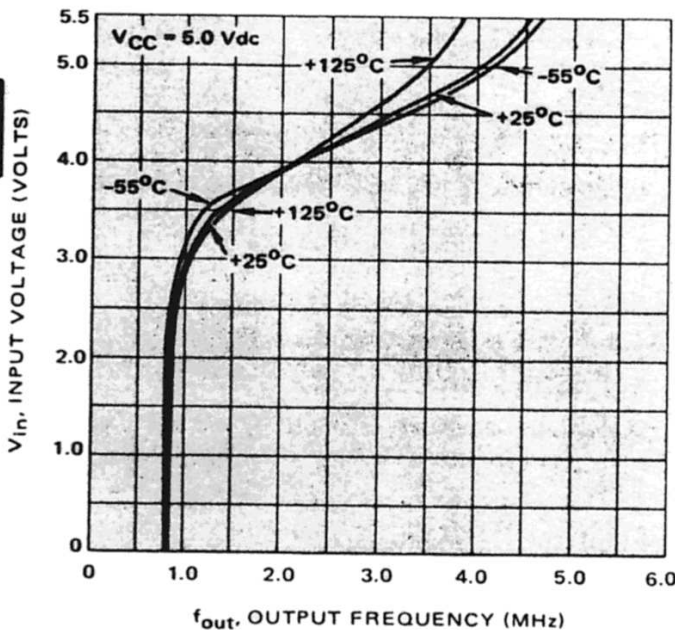


FIGURE 8 – MC4324 Input Voltage versus Output Frequency (100 pF Feedback Capacitor)

The transfer function of the VCM is given by

$$K_o = \frac{K_v}{s} \quad (45)$$

Where  $K_v$  is the sensitivity in radians per second per volt. From the curve in Figure 8,  $K_v$  is found by taking the reciprocal of the slope.

$$K_v = \frac{4 \text{ MHz} - 1.5 \text{ MHz}}{5 \text{ V} - 3.6 \text{ V}} 2\pi \text{ rad/s/V}$$

$$K_v = 11.2 \times 10^6 \text{ rad/s/V} \quad (46)$$

Thus

$$K_o = \frac{11.2 \times 10^6}{s} \text{ rad/s/V} \quad (47)$$

The  $s$  in the denominator converts the frequency characteristics of the VCM to phase, i.e., phase is the integral of frequency.

The gain constant for the MC4044/4344 phase detector is found by <sup>5</sup>

$$K_p = \frac{\text{DF High} - \text{UF Low}}{2(2\pi)} = \frac{2.3 \text{ V} - 0.9 \text{ V}}{4\pi} = 0.111 \text{ V/rad} \quad (48)$$

Since a type 2 system is required (phase coherent output) the loop transfer function must take the form of Equation 19. The parameters thus far determined include  $K_p$ ,  $K_o$ ,  $K_n$  leaving only  $K_f$  as the variable for design. Writing the loop transfer function and relating it to Equation 19

$$G(s)H(s) = \frac{K_p K_v K_n K_f}{s} = \frac{K(s+a)}{s^2} \quad (49)$$

Thus  $K_f$  must take the form

$$K_f = \frac{s+a}{s} \quad (50)$$

in order to provide all the necessary poles and zeroes for

required  $G(s)H(s)$  The circuit shown in Figure 9 is desired results.

$K_f$  is expressed by

$$K_f = \frac{R_2 C s + 1}{R_1 C s} \quad \text{for large } A \quad (51)$$

where  $A$  is voltage gain of the amplifier.

$R_1$ ,  $R_2$ , and  $C$  are then the variables used to establish overall loop characteristics.

The MC4044/4344 provides the active circuitry required to configure the filter  $K_f$ . An additional low current high impedance device or FET can be used to boost the input impedance thus minimizing the leakage current from the capacitor  $C$  between sample updates. As a result longer sample periods are achievable.

Since the gain of the active filter circuitry in the MC4044/4344 is not infinite, a gain correction factor  $K_C$  must be applied to  $K_f$  in order to properly characterize the function.  $K_C$  is found experimentally to be  $K_C = 0.5$ .

$$K_{fc} = K_f K_C = 0.5 \left( \frac{R_2 C s + 1}{R_1 C s} \right) \quad (52)$$

(For large gain, Equation 51 applies.)

The PLL circuit diagram is shown in Figure 10 and its block representation in Figure 11.

The loop transfer function is

$$G(s)H(s) = K_p K_{fc} K_o K_n \quad (53)$$

$$G(s)H(s) = K_p (0.5) \left( \frac{R_2 C s + 1}{R_1 C s} \right) \left( \frac{K_v}{s} \right) \left( \frac{1}{N} \right) \quad (54)$$

The characteristic equation takes the form

$$C.E. = 1 + G(s)H(s) = 0$$

$$= s^2 + \frac{0.5 K_p K_v R_2}{R_1 N} s + \frac{0.5 K_p K_v}{R_1 C N} \quad (55)$$

Relating Equation 55 to the standard form given by Equation 34

$$s^2 + \frac{0.5 K_p K_v R_2}{R_1 N} s + \frac{0.5 K_p K_v}{R_1 C N} = s^2 + 2 \zeta \omega_n s + \omega_n^2 \quad (56)$$

Equating like coefficients yields

$$\frac{0.5 K_p K_v}{R_1 C N} = \omega_n^2 \quad (57)$$

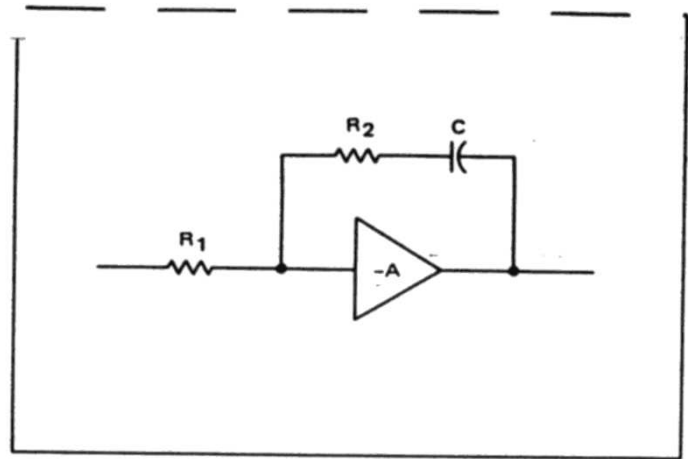


FIGURE 9 - Active Filter Design

$$\text{and} \quad \frac{0.5 K_p K_v R_2}{R_1 N} = 2 \zeta \omega_n \quad (58)$$

With the use of an active filter whose open loop gain ( $A$ ) is large ( $K_C = 1$ ), Equations 57 and 58 become

$$\frac{K_p K_v}{R_1 C N} = \omega_n^2 \quad (59)$$

$$\frac{K_p K_v R_2}{R_1 N} = 2 \zeta \omega_n \quad (60)$$

The percent overshoot and settling time are now used to determine  $\omega_n$ . From Figure 6 it is seen that a damping ratio  $\zeta = 0.8$  will produce a peak overshoot less than 20% and will settle to within 5% at  $\omega_n t = 4.5$ . The required lock-up time is 1 ms.

$$\omega_n = \frac{4.5}{1} = \frac{4.5}{0.001} = 4.5 \text{ krad/s} \quad (61)$$

Rewriting Equation 57

$$R_1 C = \frac{0.5 K_p K_v}{\omega_n^2 N} \quad (62)$$

$$= \frac{(0.5)(0.111)(11.2 \times 10^6)}{(4500)^2 (30)}$$

$$R_1 C = 0.00102$$

(Maximum overshoot occurs at  $N_{\max}$  which is minimum loop gain)

$$\text{Let } C = 0.5 \mu\text{F}$$

$$\text{Then } R_1 = \frac{0.00102}{0.5 \times 10^{-6}} = 2.04 \text{ k}\Omega$$

$$\text{Use } R_1 = 2 \text{ k}\Omega$$



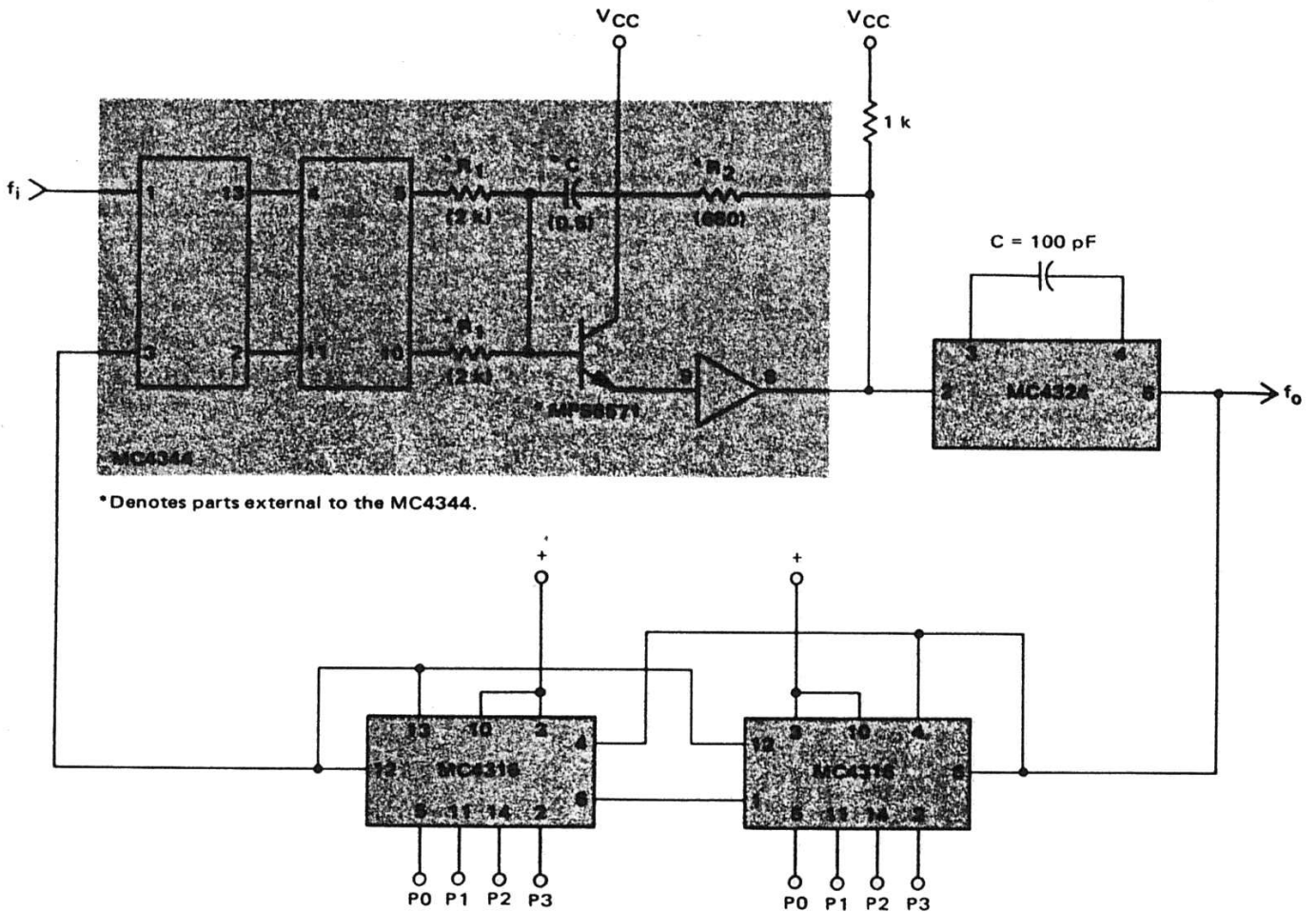


FIGURE 10 – Circuit Diagram of Type 2 Phase Locked Loop

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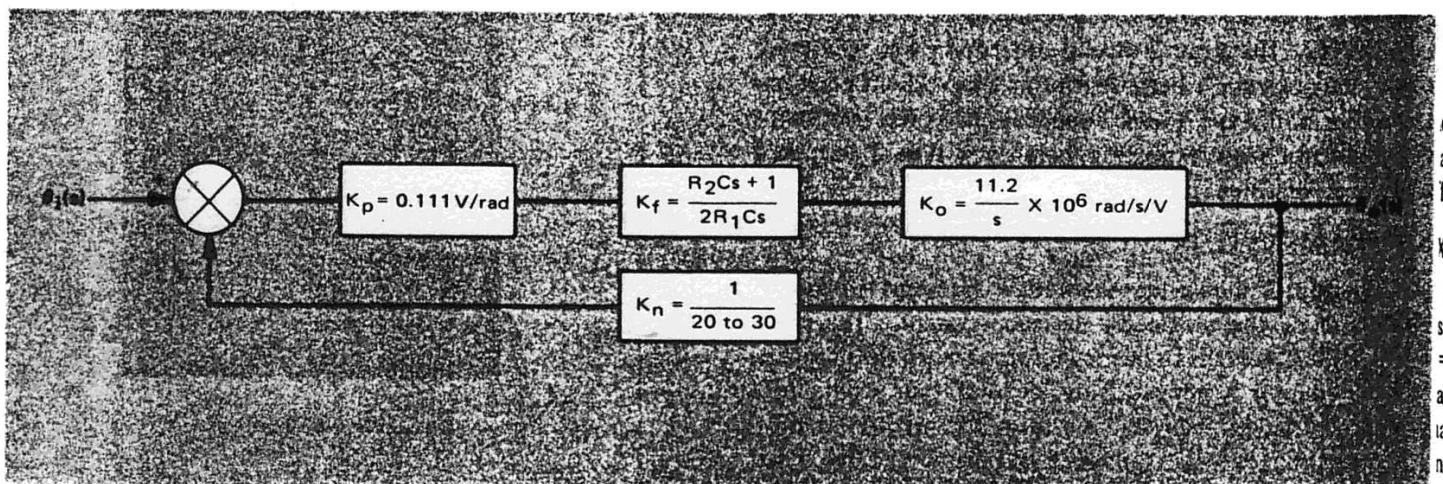


FIGURE 11 – Laplace Representation of Diagram in Figure 10

For typical selected values that  $\Omega$ .

Solving for  $R_2$  in Equation 58

$$R_2 = \frac{2\zeta \omega_n R_1 N}{K_p K_v (0.5)} = \frac{2\zeta}{C \omega_n} \quad (63)$$

$$= \frac{2(0.8)}{(0.5 \times 10^{-6})(4.5 \text{ k})}$$

$$= 711 \Omega$$

Use  $R_2 = 680 \Omega$

All circuit parameters have now been determined and the PLL can be properly configured.

Since the loop gain is a function of the divide ratio, the closed loop poles will vary in position as  $K_N$  varies. The root locus shown in Figure 12 illustrates the second loop pole variation.

The loop was designed for the programmable counter  $N = 30$ . The system response for  $N = 20$  exhibits a wider bandwidth and larger damping factor, thus reducing both the lock-up time and percent overshoot (see Figure 14).

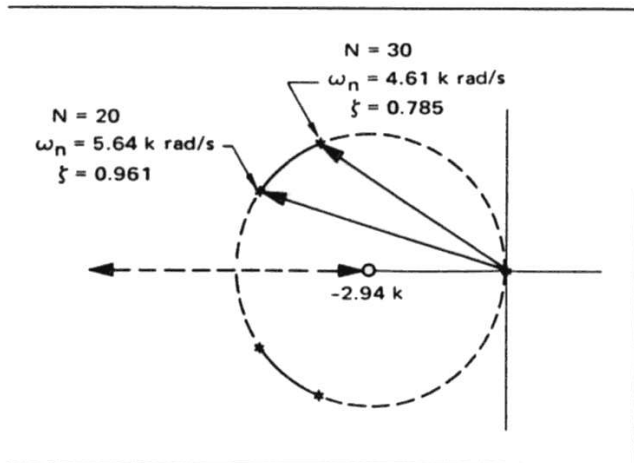


FIGURE 12 – Root Locus Variation

NOTE: The type 2 second order loop was illustrated in the design example because it provides excellent performance for both type 1 and 2 applications. Even in systems that do not require phase coherency a type 2 loop still offers an optimum design.

### EXPERIMENTAL RESULTS

Figure 13 shows the theoretical transient frequency response of the previously designed system. The curve for  $N = 30$  illustrates the frequency response when the programmable counter is stepped from 29 to 30 thus producing a change in the output frequency from 2.9 MHz to 3.0 MHz. An overshoot of 18% is obtained and the output frequency is within 5 kHz of the final value one millisecond after the divided step. The curve  $N = 20$  illustrates the output fre-

quency change when the programmable counter is stepped from 21 to 20.

Since the output frequency is proportional to the VCM control voltage, the PLL frequency response can be observed with an oscilloscope by monitoring pin 2 of the VCM. The average frequency response as calculated by the Laplace method is found experimentally by smoothing this voltage at pin 2 with a simple RC filter whose time constant is long compared to the phase detector sampling rate but short compared to the PLL response time. With the programmable counter set at 29 the quiescent control voltage at pin 2 is approximately 4.37 volts. Upon changing the counter divide ratio to 30 the control voltage increases to 4.43 volts as shown in Figure 14. A similar transient occurs when stepping the programmable counter from 21 to 20. Figure 14 illustrates that the experimental results obtained from the configured system follows the predicted results shown in Figure 13. Linearity is maintained for phase errors less than  $2\pi$ , i.e. there is no cycle slippage at the phase detector.

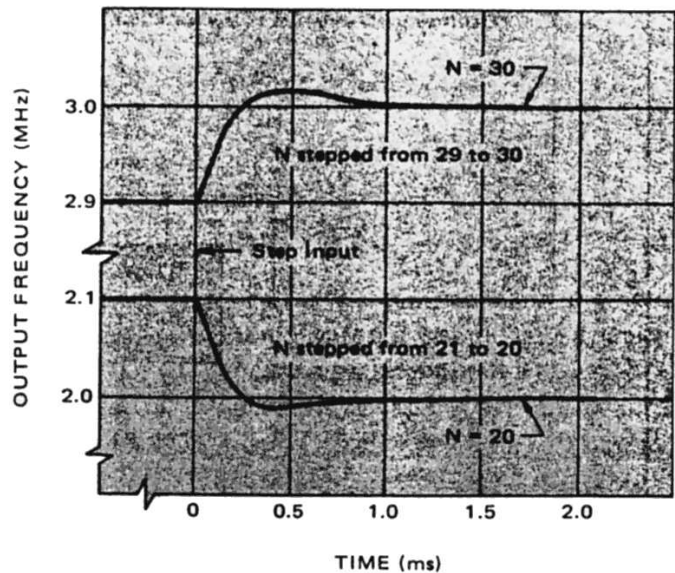


FIGURE 13 – Frequency-Time Response

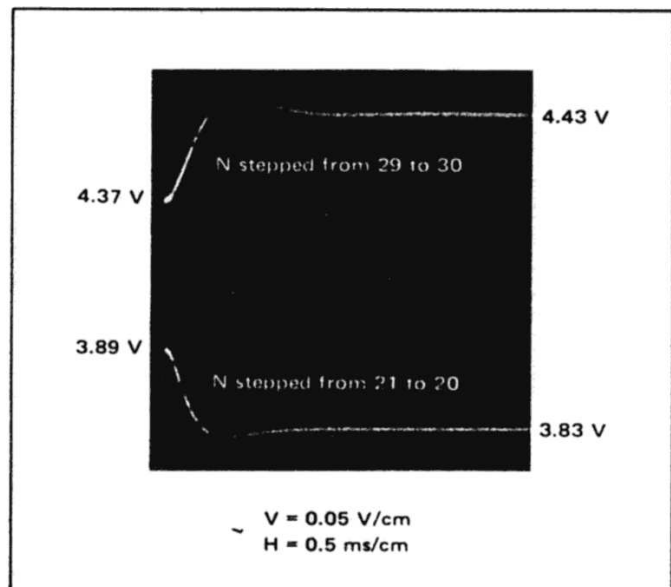


FIGURE 14 – VCM Control Voltage (Frequency) Transient

PHASE DETECTOR GAIN CONSTANT	P1 = 0.111 VOLTS PER RADIAN
VCM GAIN CONSTANT	V1 = 1.12 E+7 RAD PER VOLT
FILTER INPUT RESISTOR	R1 = 3999 OHMS (R1 <sub>0</sub> = 2k)
FILTER FEEDBACK RESISTOR	R2 = 886 OHMS
FILTER CAPACITOR	C1 = 0.5 MICROFARADS
DIVIDER VALUE	N1-N2 = 29-30
REFERENCE FREQUENCY	F1 = 100000 CPS
OUTPUT FREQUENCY CHANGE	F5 = 100000 CPS

P2 = 0.111	C2 = 0.5
V2 = 1.12 E+7	N3-N4 = 21-20
R3 = 3999 (R1 <sub>0</sub> = 2k)	F2 (F6) = 100000 (100000)
R4 = 886	

PLOT OF FUNCTIONS

(NOTE: Y(T) IS PLOTTED '+', Z(T) IS 'O', AND '0' IS COMMON)  
 FOR T: TOP = 0 BOTTOM = 0.0015 INCREMENT = 0.0005  
 FOR FCTS: LEFT = 0 RIGHT = 0.12 INCREMENT = 0.002

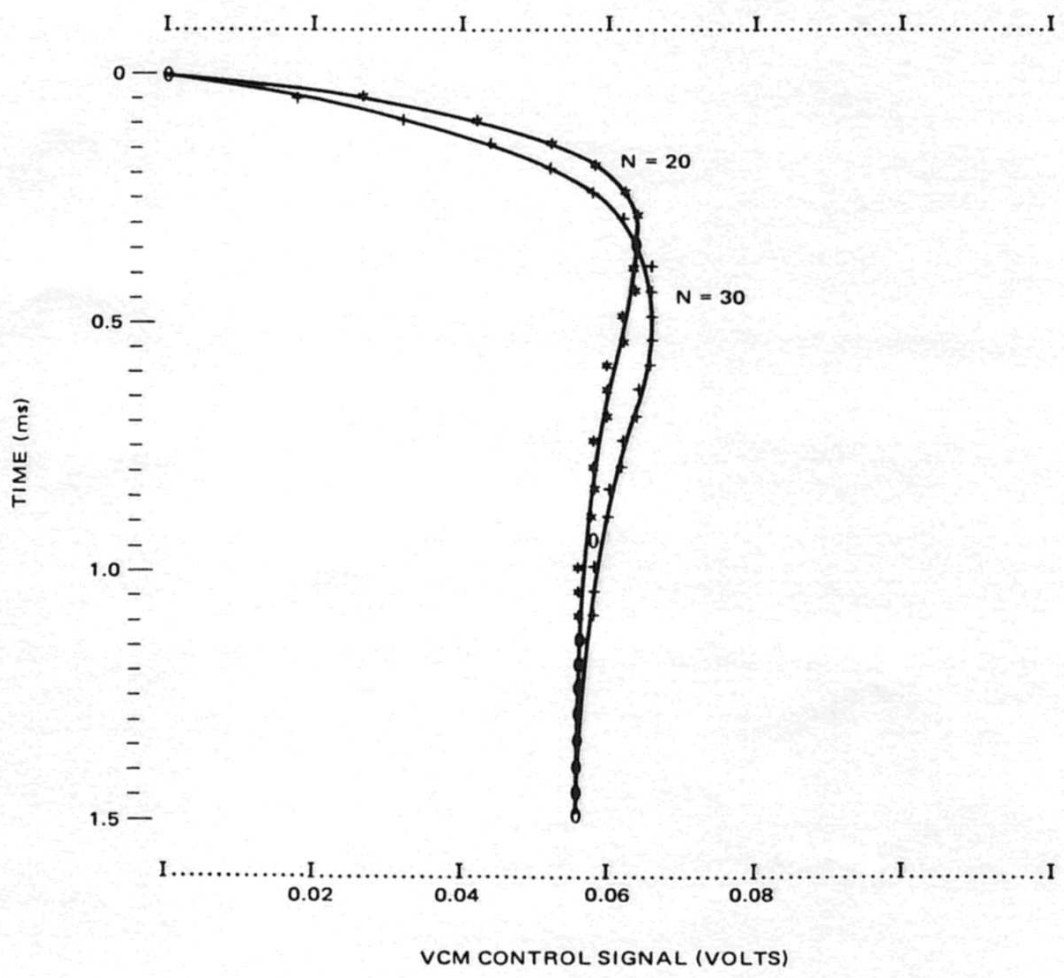


FIGURE 15 - VCM Control Signal Transient

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Figure 15 is a theoretical plot of the VCM control voltage transient as calculated by a computer program. The computer program is written with the parameters of Equations 58 and 59 (type 2) as the input variables and is valid for all damping ratios of  $\zeta \leq 1.0$ . The program prints or plots the control voltage transient versus time for desired settings of the programmable counter. The lock-up time can then be readily determined as the various parameters are varied. (If stepping from a higher divide ratio to a lower one the transient will be negative.) Figures 14 and 15 also exhibit a close correlation between the experimental and analytical results.

#### SUMMARY

This application note describes the basic control system techniques required for phase-locked loop design. Criteria for the selection of the optimum type of loop and methods for establishing the desired performance characteristics are presented. A design example is illustrated in a step-by-

step approach along with the comparison of the experimental and analytical results.

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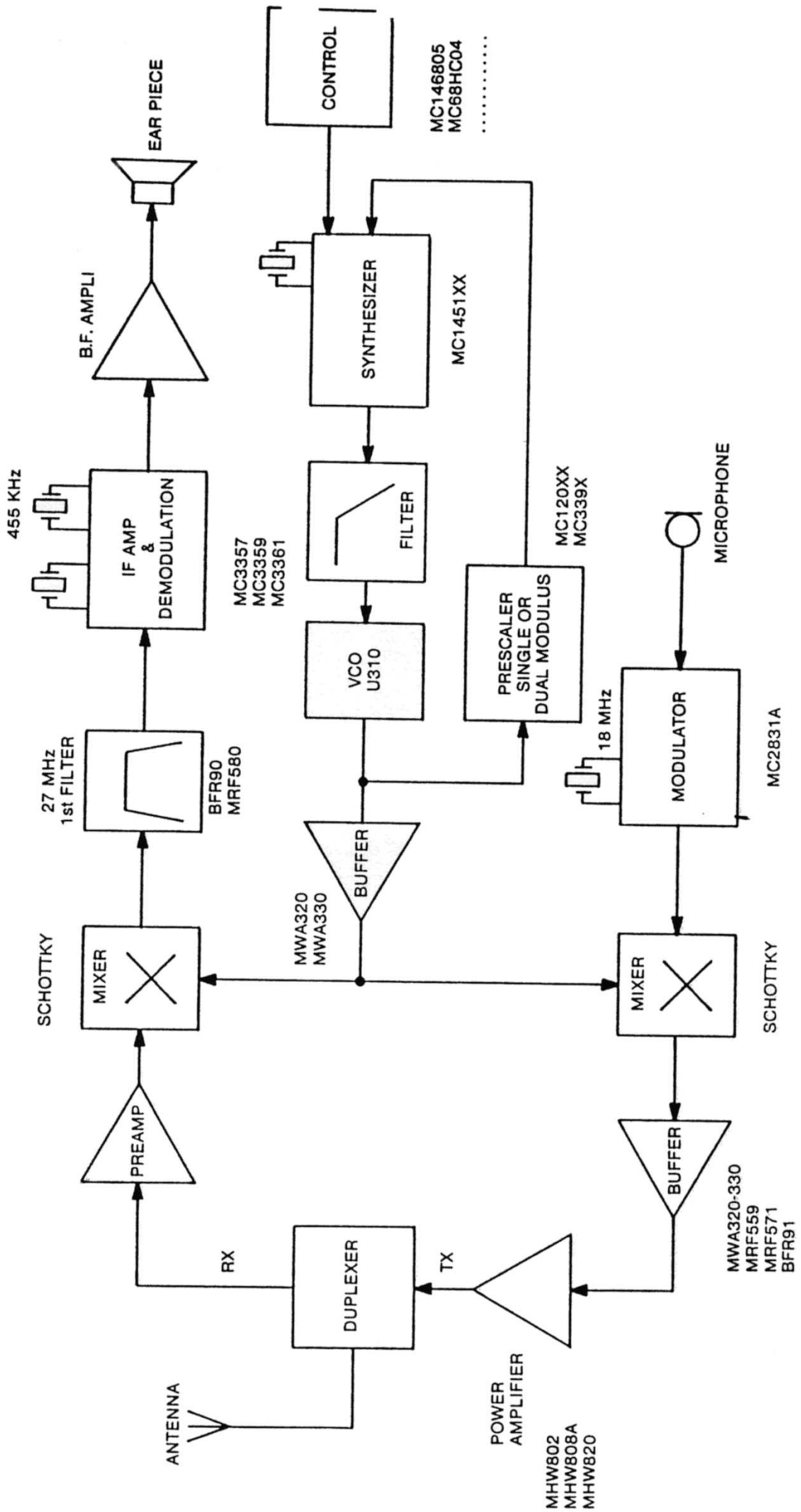
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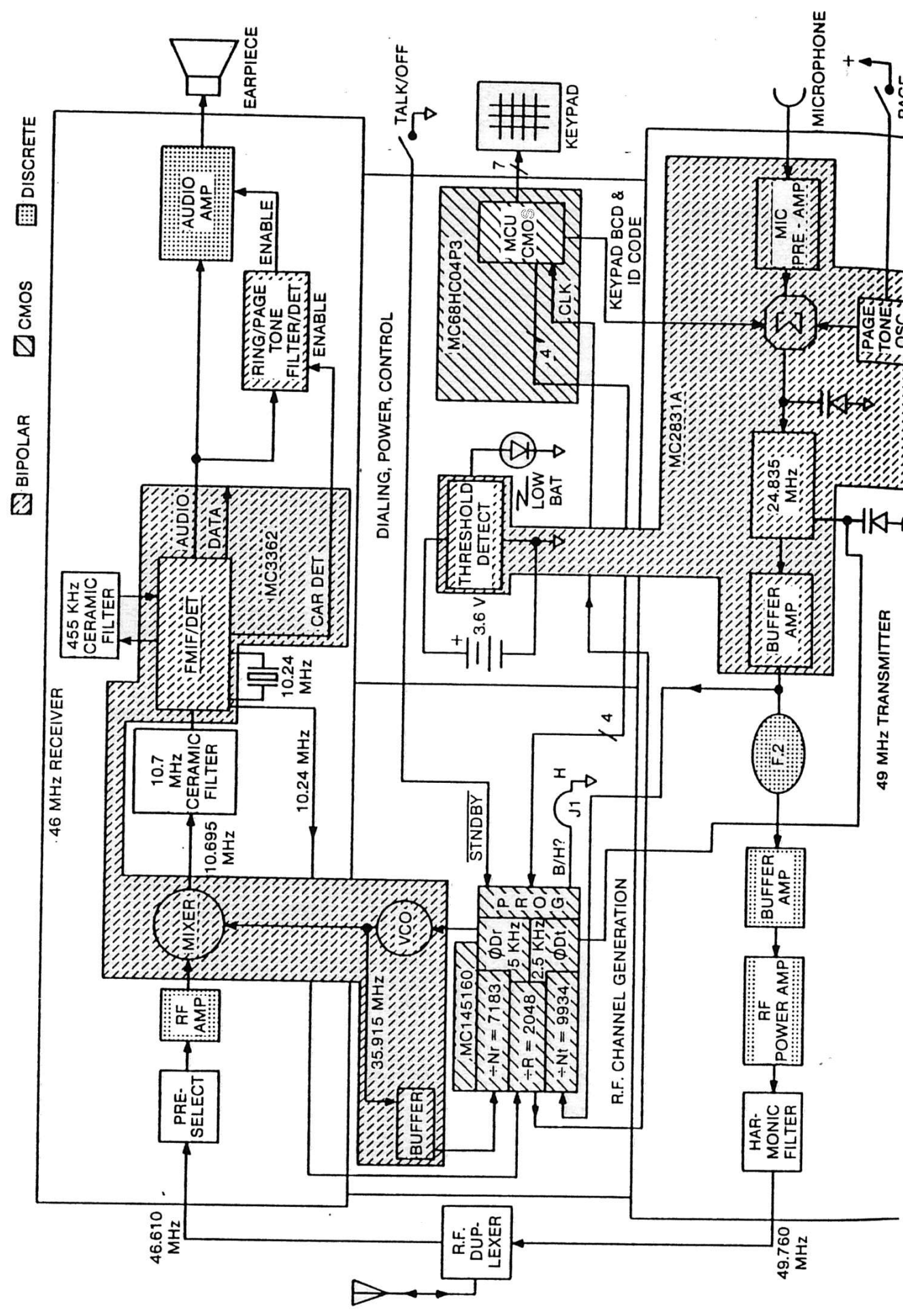
## **Typical Applications**



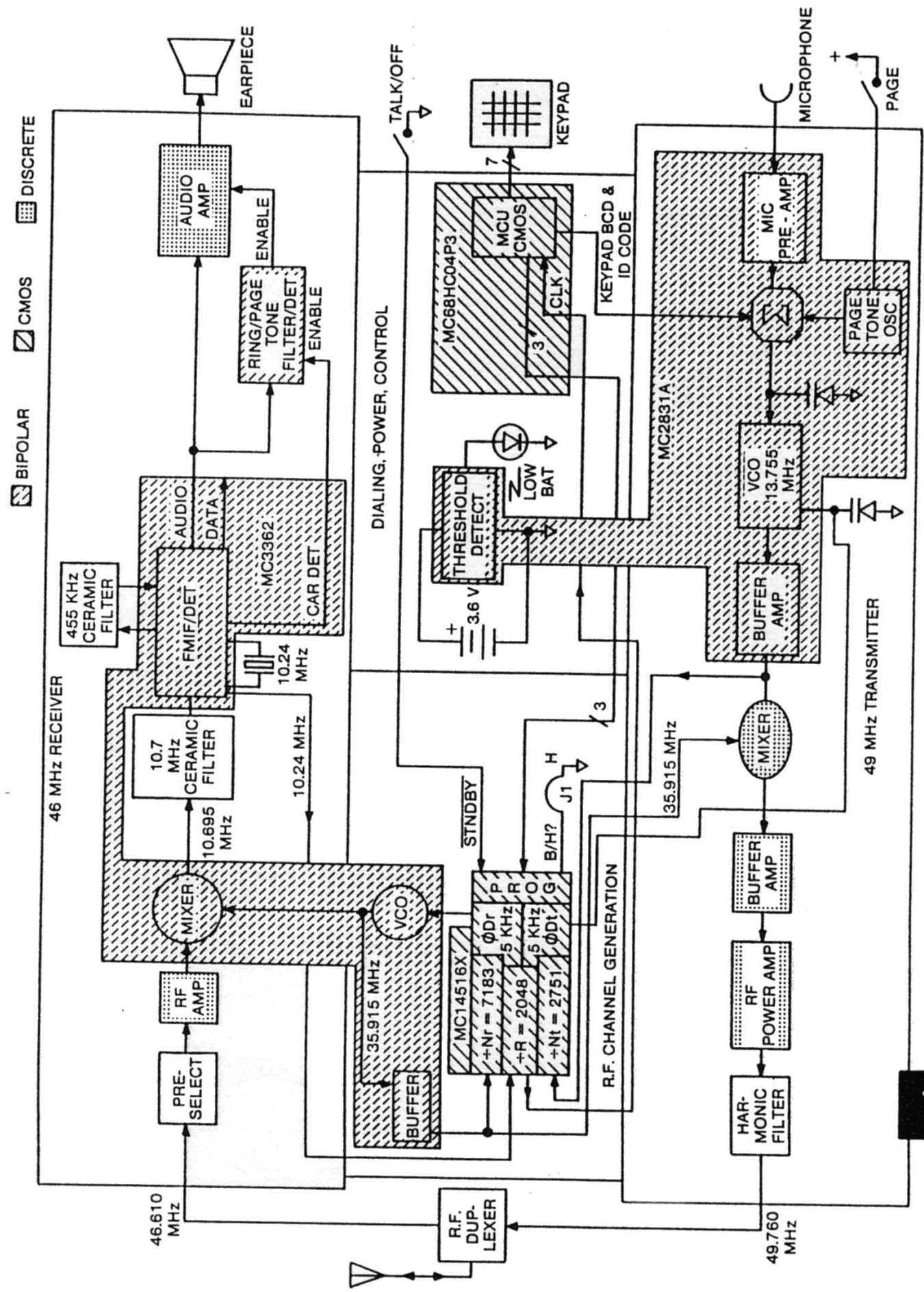
# CORDLESS TELEPHONE USING ONE PHASE LOCKED LOOP



APPLICATION OF DUAL LOOP SYNTHESIZER TO CORDLESS PHONE HANDSET  
 RECEIVER INJECTION AND HALF TRANSMIT FREQ. OSCILLATORS



APPLICATION OF DUAL LOOP SYNTHESIZER TO CORDLESS PHONE HANDSET  
(RECEIVER INJECTION AND OFFSET OSCILLATORS)







# **List of Application Notes and Engineering Bulletins**




## APPLICATION NOTES

Device	Description
AN178A/D	EPICAP Tuning Diode Theory and Application . . . . .
AN182/D	A Method of Protecting Thermal Stability . . . . .
AN210/D	FM Modulation Capabilities of EPICAP VVC's . . . . .
AN211/D	Field Effect Trans. in Theory and Practice . . . . .
AN215A/D	RF Small Signal Design, using Two Part Parameters . . . . .
AN220/D	FET's in Chopper and Analog Switching Circuits . . . . .
AN238/D	Trans Mixer Design using 2 Part Parameters . . . . .
AN249/D	Designing around the Tuning Diode Inductance . . . . .
AN417B/D	IC Crystal Controlled Oscillators . . . . .
AN484A/D	Medium Power Audio Amps using Comptrans . . . . .
AN485/D	H/P Audio Amps with Short Circuit Protection . . . . .
AN513/D	A High Gain I/C RF IF Amp with Wide Range AGC . . . . .
AN531/D	MC1596 Balanced Modulator . . . . .
AH535/D	Phase Locked Loop Design Fundamentals . . . . .
AN556/D	A New Generation of Integrated Avionic Synthesizers . . . . .
AN577/D	Design Techniques for an 80 Watt, 175 MHz Transmitter 12.5 V Operation . . . . .
AN595/D	25 Watt and 10 Watt VHF Marine Band Transmitter . . . . .
AN728/D	13 Watt Microstrip Amplifier for 220-225 MHz Operation . . . . .
AN742/D	A 200 MHz Autoranging MECL-HCMOS Frequency Counter . . . . .
AN749/D	Broadband Transformers and Power Combining Techniques for RF . . . . .
AN790/D	Thermal Rating of RF Power Transistors . . . . .
AN791/D	A Simplified Approach to VHF Power Amplifier Design . . . . .
AN793/D	A 15 Watt AM Aircraft Transmitter Power Amplifier using Low Cost Plastic Transistors . . . . .
AN827/D	The Technique of Direct Programming by using a Two Modulus Prescaler . . . . .
AN860/D	Power MOSFET versus Bipolar Transistors . . . . .
AN878/D	VHF MOS Power Application . . . . .
AN883/D	A Radio Set Phase Locked Loop (PLL) using a MC6805T2 Single Chip Micro Computer . . . . .
AN918/D	Paralleling Power MOSFETS in Switching Applications . . . . .
TDT101B/D	A 60 W, 100 KHz FET Switcher . . . . .

# ENGINEERING BULLETINS

Device	Description
EB17A/D	Simple VHF Broadband Design uses CQ Transistor . . . . .
EB22/D	Economical 225 MHz Receiver Front End Employs FET . . . . .
EB46/D	Simplified ?? Watt VHF Amp . . . . .
EB53/D	Two VHF High Band Gain Blocks from 20 DB 30 W Ampli Chain . . . . .
EB57/D	An Economical FM Transmitter Voice Processor from a Single IC . . . . .
EB59/D	Predict Frequency Accuracy for MC12060 and MC12061 . . . . .
EB60/D	VCO and VCXO Designs using MC12060 and MC12061 Oscillators Circuits . . . . .
EB63/D	140 W Amateur Radio Linear Amp 2-30 MHz . . . . .
EB70/D	Frequency Multiplication Simplified by Internal Shield in MRF629 . . . . .
EB74/D	A 10 W 225-500 MHz Amp MRF 331 . . . . .
EB77/D	A 60 W 225-400 MHz Amp 2N6439 . . . . .
EB89/D	A 1 W, 2.3 GHz Amplifier . . . . .
EB90/D	Low Cost VHF Amp has Broadband Performance . . . . .
EB93/D	60 W VHF Amplifier uses Splitting/Combining Techniques . . . . .
EB104/D	Get 600 Watt RF from Four Power FETs . . . . .
EB105/D	A 30 Watt, 800 MHz Amplifier Design . . . . .
EB107/D	Mounting Considerations for Motorola RF Power Modules . . . . .
EB109/D	Low Cost VHF Device gives Broadband Performance at 3 Watt Output . . . . .

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